

# **Elmer GUI Tutorials**

Peter Råback

CSC – IT Center for Science

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# Elmer GUI Tutorials

## About this document

The Elmer GUI Tutorials is part of the documentation of Elmer finite element software. Elmer GUI Tutorials gives examples on the use of Elmer in different field of continuum physics. Also coupled problems are included.

All these tutorials assume the use of ElmerGUI, the graphical user interface of Elmer. There are also older tutorials in the Elmer non-GUI Tutorials that may be used by advanced users.

The present manual corresponds to Elmer software version 7.0. Latest documentations and program versions of Elmer are available (or links are provided) at <http://www.csc.fi/elmer>.

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# Instructions for the GUI tutorials

Here are some instructions for following the GUI tutorials:

- All the needed input files should be available among the `ElmerGUI/samples` directory that should have come with the installation. Look under a subdirectory named after the suffix of the sample file.
- The instructions written in `verbatim` refer to operations with the GUI. Intendation means step in the menu hierarchy. The instructions should not be mixed with those in the command file.
- The menu structure for the default set of equations is located in directory `edf`, there are a few additional ones in directory `edf-extra`. These may be copied to the directory `edf` permanently, or be appended to the menus while running the ElmerGUI.
- The default menu structure may differ from the configuration used when writing the tutorial. Hence the user is encouraged to check by herself whether the menu structures exist or not.
- After having once defined the case you may go to the working directory and launch ElmerSolver from command-line. There you may edit the `.sif` file to alter the parameters.
- Manual alteration to the `sif` file will not be communicated to the ElmerGUI project. All editions will be overrun by the GUI when saving the project.
- The cases have been run a number of times but errors are still possible. Reporting them to `elmer-adm@csc.fi`, for example, is greatly appreciated.

# Tutorial 1

## Heat equation – Temperature field of a solid object

**Directory:** TemperatureGenericGUI

**Solvers:** HeatSolve

**Tools:** ElmerGUI,netgen,OpenCascade

**Dimensions:** 3D, Steady-state

### Problem description

This tutorial tried to demonstrate how to solve the heat equation for a generic 3D object. The solid object (see figure 1.1) is heated internally by a heat source. At some part of the boundary the temperature is fixed. Mathematically the problem is described by the Poisson equation

$$\begin{cases} -\kappa\Delta T = \rho f & \text{in } \Omega \\ T = 0 & \text{on } \Gamma \end{cases} \quad (1.1)$$

where  $\kappa$  is the heat conductivity,  $T$  is the temperature and  $f$  is the heat source. It is assumed that density and heat conductivity are constants.

To determine the problem we assume that the part of the boundary is fixed at  $T_0 = 293$  K, the internal heat generation is,  $h = 0.01$  W/kg, and use the material properties of aluminium.

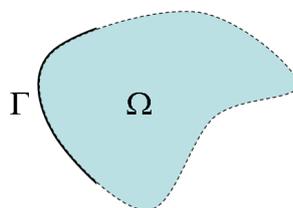


Figure 1.1: Generic object being heated

## Solution procedure

Start ElmerGUI from command line or by clicking the icon in your desktop. Here we describe the essential steps in the ElmerGUI by writing out the clicking procedure. Tabulation generally means that the selections are done within the window chosen at the higher level.

The geometry is given in step format in file `pump_carter_sup.stp` in the `samples/step` directory of ElmerGUI. This file is kindly provided at the AIM@SHAPE Shape Repository by INRIA. The heat equation is ideally suited for the finite element method and the solution may be found even at meshes that for some other problems would not be feasible. Therefore you may easily experiment solving the same problem with different meshes. If you lack OpenCascade you might try to solve a similar problem with the `grd` files `angle3d.grd`, `angles3d.grd`, `bench.grd`, or `cooler.grd`, for example.

The CAD geometry defined by the step file is transformed on-the-fly by OpenCascade library into a stl file for which `nglib` creates tetrahedral volume discretization. You may also use the `tetlib` library (`tetgen`) if you have installed it as a plug-in.

Load the input file:

```
File
  Open -> pump_carter_sup.stp
```

The meshing will take a minute or two. You should obtain your mesh and may check in the number of element in the `Model` summary. With `netgen` the default setting generates 8371 nodes and 36820 tetrahedral elements. Visual inspection reveals that the mesh is not quite satisfactory in geometric accuracy. We choose to modify the mesh by altering the settings in the following way.

```
View -> Cad model...
  Model -> Preferences...
    Restrict mesh size on surfaces by STL density = on
    Apply
Mesh -> Remesh
```

The meshing a take a minute or two. The modified mesh should include 16159 nodes and 65689 tetrahedral elements and be more appealing to the eye. In order to affect the mesh density study the command-line options of the `netgen` manual. Here we continue with the default mesh.

We want to set the temperature at the inside of the holes and in that aim you may join the three boundaries (see figure 1.2). For that aim we may choose the six pieces that constitute the boundaries as shown in the picture by pressing the `Ctrl`-key down.

```
Mesh
  Unify Surface
```

After we have the mesh we start to go through the `Model` menu from the top to bottom. In the `Setup` we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 3-dimensional cartesian coordinates and in steady-state. Only one steady-state iteration is needed as the case is linear.

```
Model
  Setup
    Simulation Type = Steady state
    Steady state max. iter = 1
```

Choose `Apply` to close the window.

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have one set only one equation – the heat equation.

When defining Equations and Materials it is possible to assign the to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore its easier to assign the Equation and Material to it directly, whereas the active boundary is chosen graphically.

For the linear system solvers we are happy to use the defaults. One may however, try out different preconditioners (`ILU1,..`), for example.

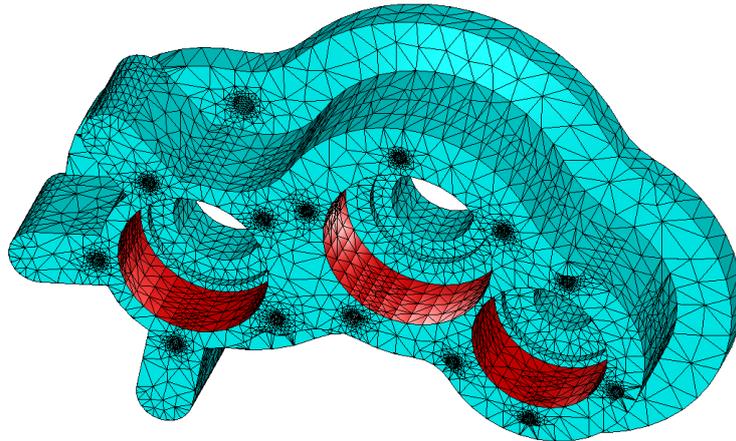


Figure 1.2: The computational mesh showing the three joined boundaries

```

Model
  Equation
    Add
      Name = Heat Equation
      Apply to bodies = Body 1
      Heat Equation
        Active = on
    Add
  OK

```

The Material section includes all the material parameters. They are divided to generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the mass. Other properties assume a physical law, such heat conductivity. We choose Aluminium from the Material library which automatically sets for the needed material properties.

```

Model
  Material
    Add
      Material library
        Aluminium
      Apply to bodies = Body 1
    Add
  OK

```

A Body Force represents the right-hand-side of a equation that in this case represents the heat source.

```

Model
  Body Force
    Add
      Name = Heating
      Heat Source = 0.01
      Apply to bodies = Body 1
    Add
  OK

```

No initial conditions are required in steady state case.

In this case we have only one boundary and set it to room temperature. First we create the boundary condition

```
Model
  BoundaryCondition
    Add
      Heat Equation
        Temperature = 293.0
      Name = RoomTemp
    Add
      OK
```

Then we set the boundary properties

```
Model
  Set boundary properties
```

Choose the defined group of three boundaries by clicking with the mouse and apply the condition for this boundary.

```
Boundary condition
  RoomTemp
```

For the execution ElmerSolver needs the mesh files and the command file. We have know basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```
Sif
  Generate
  Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. In saving the project all the necessary files for restarting the case will be saved to the destination directory.

```
File
  Save Project
```

After we have successfully saved the files we may start the solver

```
Run
  Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. As the case is linear only one iteration was required for the solution and the second one just is needed to check the convergence. The norm of the solution should be around 432.4 K (with the default tetgen mesh 389.8 K, respectively).

Note: if you face problems in the solution phase and need to edit the setting, always remember to regenerate the sif file and save the project before execution.

## Postprocessing

To view the results we may use the ElmerPost postprocessor or start the the internal VTK widget as is done here,

```
Run
  Postprocessor (VTK)
```

The default configuration shows just the object. To color the surface with the temperature choose

```
Surfaces
  Surface: Temperature
  Apply
```

The maximum temperature should be about 586.5 K. You may turn on opacity in order to see through the object, 10-20% is a good value. This way you'll able to see some isosurfaces that you might want to define. Some examples of the visualizations may be seen in figure 1.3.

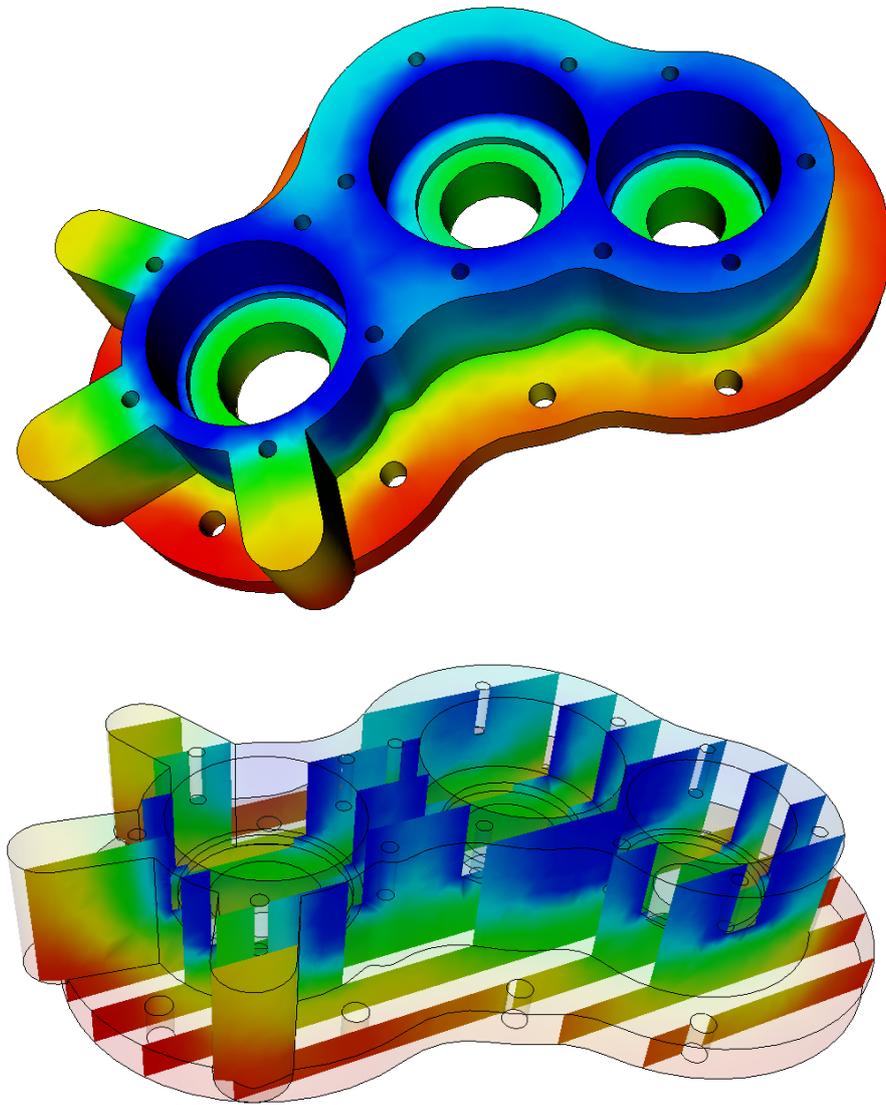


Figure 1.3: The temperature distribution of the solid object domain as visualized using the VTK-based postprocessor

## Tutorial 2

# Linear elasticity equation – Loaded elastic beam

**Directory:** ElasticBeam3D

**Solvers:** StressSolve

**Tools:** ElmerGUI

**Dimensions:** 3D, Steady-state

### Case definition

Assume a homogenous, elastic beam being rigidly supported on one end. On the other end it is subjected with a load of 2000 N resulting from an attached object in the gravitational field. The gravity affects also the beam itself. The length of the beam is 1 m and the thickness is 0.05 m, and the width 0.1 m. Material properties of the beam are those of dry pine timber: Poisson ratio 0.37, Young's modulus  $10 \cdot 10^9 \text{N/m}^2$ , and density  $550 \text{kg/m}^3$ . The problem is to solve the displacement and stress field of the beam. Here the `StressSolve` routine based on the linear theory of elasticity is applied.

### Solution procedure

The mesh is given in ElmerGrid format in file `beam3d.grd`, load this file.

File

Open -> `beam3d.grd`

You should obtain your mesh and may check that it consists of 6073 nodes and of 1200 quadratic hexahedral elements. The second order elements give improved accuracy compared to the first order elements as they avoid the phenomenon known as locking.

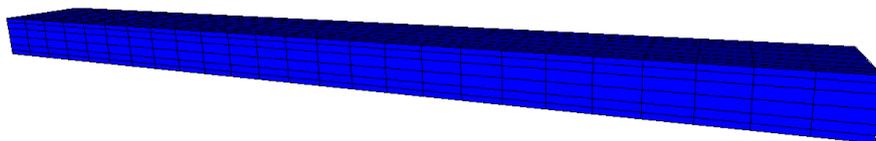


Figure 2.1: The mesh used in the computations

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried in steady-state in 3-dimensional cartesian coordinates.

```
Model
  Setup
    Simulation Type = Steady state
    Steady state max. iter = 1
```

In the Equation section we choose the relevant equations which in this case only includes the Linear elasticity equation which solves the problem according to linear elastic theory. We also want to compute the stresses as a post-processing step. For the linear system solvers we change the default settings in order to obtain a better convergence in this case. As the equation is fully linear we also eliminate the nonlinear iteration loop.

```
Model
  Equation
    Name = Elasticity
    Apply to Bodies = Body 1
    Linear elasticity
      Active = on
      Calculate Stresses = on
    Edit Solver Setting
      Linear System
        Method = Iterative / GCR
        Preconditioning = ILU1
      Nonlinear system
        Max. iterations = 1
    Apply
  Add
  OK
```

The Material section includes all the material parameters. They are divided to generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the mass. Other properties assume a physical law, such as Young's modulus and Poisson ratio.

```
Model
  Material
    Name = Pine
    General
      Density = 550
    Linear Elasticity
      Youngs Modulus = 10.0e9
      Poisson ratio = 0.37
    Apply to Bodies = Body 1
  Add
  OK
```

In this case there is a body force i.e. the gravity acting on the beam. We assume that the gravity points to the negative  $y$  direction.

```
Model
  BodyForce
    Name = Gravity
    Linear Elasticity
      Force 2 = $ -9.81 * 550
    Apply to Bodies = Body 1
```

```
Add
OK
```

Here we use a MATC expression for computing the volume force. This expression is constant and is computed when the command file is interpreted.

Convergence should be obtained with the default initial condition i.e. zero for all fields, hence no initial condition is applied.

The first boundary condition fixes the beam rigidly at the wall. The second boundary condition distributes the load of 2000 N uniformly on the area of  $5.0e-3 \text{ m}^2$ .

```
Model
BoundaryCondition
  Name = Wall
  Linear elasticity
    Displacement 1 = 0.0
    Displacement 2 = 0.0
    Displacement 3 = 0.0
Add
New

Name = Mass
Linear elasticity
  Force 2 = -4.0e5
Add
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

```
Model
Set boundary properties
  Choose the wall end of the beam -> set boundary condition Wall
  Choose the other end of the beam -> set boundary condition Mass
```

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```
Sif
Generate
Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

```
File
Save Project
```

After we have successfully saved the files we may start the solver

```
Run
Start solver
```

The simulation may take a minute or so depending on the speed of the processor. This time the convergence monitor does not have a meaningful output since the of the different steps only one is related to the actual solution and the six other ones to the computation of stresses with the Galerkin method.

## Results

When there are some results to view we may start the postprocessor, this time we use ElmerPost.

```
Run
  Start postprocessor
```

As a result the absolute value of maximum displacement is shown. The maximum displacement is 6.36 cm. To visualize the displacement in the geometry using ElmerPost can be done with the following command in the Elmer-Post command line.

```
math n0=nodes
math nodes=n0+Displacement
```

To redraw the picture with new settings use the rightmost icon on the top row. The resulting picture is shown in Fig 2.2. Note that the displacement are so large that the assumption of linearity may be severely

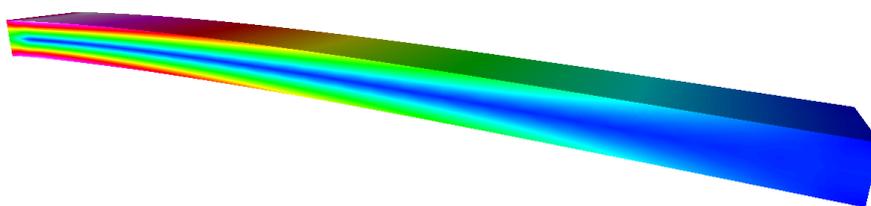


Figure 2.2: The displaced shape of the elastic beam colored with the von Mises stresses

questioned. When further increasing the loading one should resort to a solver that is able to catch the geometric nonlinearities.

### Extra task: Gravity in $x$ direction

The beam should be more rigid if the beam is oriented differently. For that aim, change the direction of gravity to orient in the negative  $x$ . Change the body force

```
Model
  BodyForce
    Linear Elasticity
      Force 1 = $ -9.81*550
    Update
  OK
```

and the boundary condition

```
Model
  BoundaryCondition
    Linear elasticity
      Force 1 = -4.0e5
    Update
  OK
```

The rigidity should scale as  $dh^3$  and hence the maximum displacement should be reduced roughly to one quarter of the original.

## Tutorial 3

# Smitc solver – Eigenmodes of an elastic plate

**Directory:** ElasticPlateEigenmodesGUI

**Solvers:** SmitcSolver

**Tools:** ElmerGUI

**Dimensions:** 2D, Eigenmode

### Problem description

For thin elastic structures it is often advisable to use dimensionally reduced models i.e. study plates or shells. In this tutorial we compute the few lowest eigenmodes of an elastic plate. Our geometry is a simple pentagon which (compared to a square) eliminates some of the trivial symmetries. The pentagon is rigidly fixed at all boundaries.

For more details on the solver we refer to the documentation of Smitc solver in the Elmer Models Manual.

### Solution procedure

Start `ElmerGUI` from command line or by clicking the icon in your desktop. Here we describe the essential steps in the ElmerGUI by writing out the clicking procedure. Tabulation generally means that the selections are done within the window chosen at the higher level.

Before we can start the set-up we should make sure that the menus for Smitc solver are present. If not, they may be found in file

```
$ELMERHOME/bin/edf-extra/elasticplate.html
```

To load these definitions do the following

```
File
  Definitions
    Append -> choose the file
```

To see what kind of new menu structures you got you may play around with viewer collapsing and opening. Note that if you want to load an existing project you should load the xml-definitions that were used in creating the project. Therefore it may be best to place all actively used menu definitions in directory

```
$ELMERHOME/bin/edf
```

When the menu structures for plate solver are there we are ready to continue. The mesh is given in 2d netgen format in file `pentagon.grd` in the samples directory of ElmerGUI, load this file.

```
File
  Open -> pentagon.in2d
```

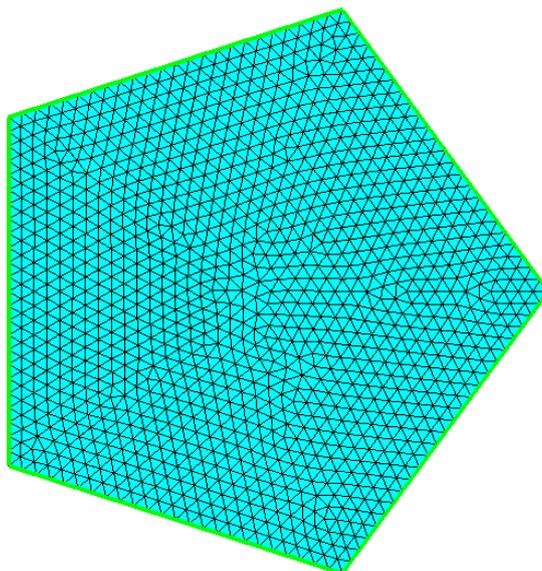


Figure 3.1: The finite element mesh in ElmerGUI

You should obtain a pentagon consisting of 5 triangles. To increase the number of elements change the parameters passed on to the nglib library by going to

```
Mesh
  Configure
    nglib / Max H: 0.05
```

You may check in the Model summary window that it consists of 1199 nodes and 2276 linear triangles. If the mesh was successfully imported your window should look something in figure 3.1.

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 2-dimensional cartesian coordinates and in steady-state (also used for eigenmodes). Only one steady-state iteration is needed as the case is linear.

```
Model
  Setup
    Simulation Type = Steady state
    Steady state max. iter = 1
  Apply
```

In the equation section we choose the relevant equations and parameters related to their solution. When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore it's easier to assign the Equation and Material to it directly.

For the solver setting we need to activate the eigen mode computation. We also choose the direct umfpack solver which for small 2D problems often performs great.

```
Model
  Equation
    Add
      Name = Plate Equation
      Apply to bodies = 1
```

```

Elastic Plates
  Active = on
  Edit Solver Settings
    Solver Specific Options
      Eigen Analysis = on
      Eigen System Values = 10
    Linear System
      Direct = on
      Umfpack
Add
OK

```

The Material section includes all the material parameters. They are divided to generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the mass. Other properties assume a physical law, such as heat Youngs modulus. As our problem is academic in nature we choose some simple ideal parameters but data from material database could also be used instead.

```

Model
  Material
    Add
      Name = Ideal
      Apply to bodies = 1
      General
        Density = 1000.0
      Elastic Plates
        Youngs Modulus = 1e9
        Poisson ratio = 0.3
        Thickness = 0.001
        Tension = 0.0
    Add
  OK

```

A Body Force represents the right-hand-side of a equation i.e. external forces. In eigenmode analysis no body forces are used. Nor are any Initial conditions required.

In this case all the boundaries are rigidly fixed we set all the components of the solution field to be zero. The 1st component is the displacement in the normal direction while the 2nd and 3rd components are its derivatives in  $x$  and  $y$  directions.

```

Model
  BoundaryCondition
    Add
      Elastic Plates
        Deflection 1 = 0.0
        Deflection 2 = 0.0
        Deflection 3 = 0.0
      Name = Fixed
      Apply to boundaries = 1 2 3 4 5
    Add
  OK

```

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```

Sif
  Generate
  Edit -> look how your command file came out

```

Before we can execute the solver we should save the files in a directory. In saving the project all the necessary files for restarting the case will be saved to the destination directory.

```
File
  Save Project
```

After we have successfully saved the files we may start the solver

```
Run
  Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. In this case there is just one iteration and thus no curve appears.

## Results

The resulting eigenvalues are shown in table 3.1. Note that some eigenmodes are degenerated but as the finite element mesh is not perfectly symmetric there will be minor differences in the eigenvalues.

Table 3.1: Ten lowest eigenvalues for the pentagon plate

No	$\omega^2$
1	18.9
2,3	81.3
4,5	214.5
6	281.1
7, 8	472.5
9, 10	621.0

Note: if you face problems in the solution phase and need to edit the setting, always remember to save the project before execution.

To view the results we may start the ElmerPost or use the internal VTK widget, as is done here

```
Run
  Postprocessor (VTK)
```

To show the 1st component

```
Surfaces
  Control / Surface: Deflection.1
  Apply
  OK
```

The default configuration shows only the 1st eigenmode. To get all the eigenmodes do the following:

```
File
  Read input file
  Timesteps / End: 10
  Apply
  OK
```

To go through all eigenmodes (treated here as timesteps)

```
Edit
  Time step control
  Loop
```

Here you may also save the pictures to files frame\*.png by activating the checkbox. In figure 3.2 the lowest eigenmodes are depicted.

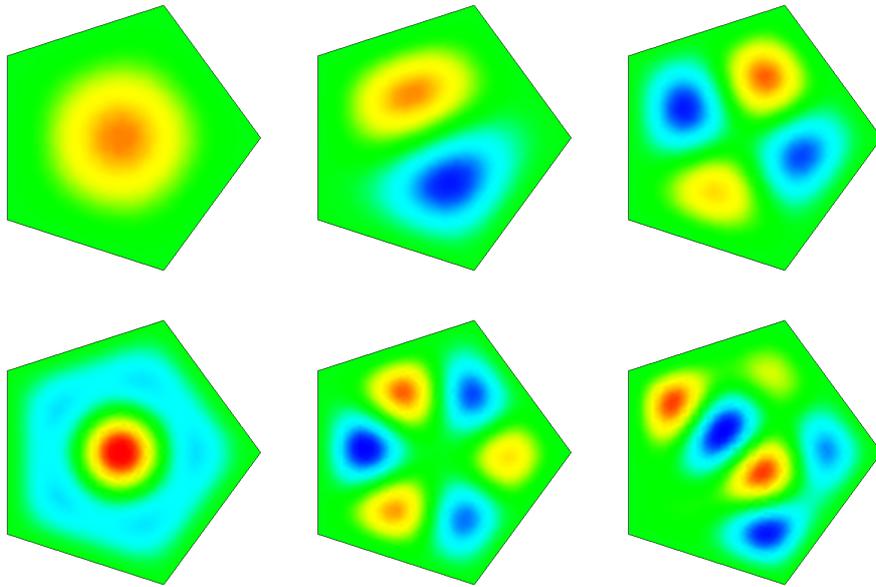


Figure 3.2: The 1st, 2nd, 4th, 6th, 7th and 9th eigenmode of the plate

### Extra task

You may test the effect of pre-stressing by altering the Tension material parameter.

There are other similar geometries that you could use i.e. `hexagon.in2d`, `heptagon.in2d`, `octagon.in2d`. When the number of vertices is increased the eigenvalues should slightly decrease.

## Tutorial 4

# Electrostatic equation – Capacitance of two balls

**Directory:** CapacitanceOfTwoBalls

**Solvers:** StatElecSolver

**Tools:** netgen,ElmerGUI

**Dimensions:** 3D, Steady-state

### Case definition

This case presents the solution of the capacitance of perfectly conducting balls in free space. A voltage difference between the balls results to electric charge being introduced to the system. The balls have also self-capacitance that comes from the voltage difference with the far field. Therefore a symmetric capacitance matrix with of size  $2 \times 2$  needs to be solved. The capacitances may be computed from two different voltage configurations. For both the electrostatic equation is solved automatically.

The problem does not have an analytical solution in a closed form. However, the cross-capacitance between the balls may be approximated from the series solution [?, Ch. A.3]:

$$C_{12} = 4\pi\epsilon \frac{a^2}{d} \left( 1 + \frac{a^2}{d^2 - 2a^2} + \frac{a^4}{d^4 - 4d^2a^2 + 3a^4} + \dots \right) \quad (4.1)$$

and the self-capacitance from

$$C_{10} = C_{20} = 4\pi\epsilon a \left( 1 - \frac{a}{d} + \frac{a^2}{d^2 - a^2} + \frac{a^3}{d^3 - 2da^2} + \dots \right) \quad (4.2)$$

Let's mark  $\tilde{C} = C/\epsilon$ . In this case  $\tilde{C}_{12} \approx 1.191$  and  $\tilde{C}_{10} \approx 5.019$ . Unfortunately the error bounds are not given.

In this particular case the balls are assumed to have a radius of  $a = 0.5$  and they are placed at distance  $d = 2$  apart from each other (measured from the ball origins).

### Meshing

In this case meshing is performed with the graphical user interface of netgen. Netgen creates tetrahedral quality meshes and provides a native output for Elmer. At the time of writing this tutorial the quadratic elements had some problems with numbering but these should not affect the linear elements.

The file is given as netgen geometry format in file `TwoBallsInBall.geo`. The geometry definition includes the two smaller balls inside a bigger ball. Ultimately the bigger ball would be infinitely large. As this is impossible here we choose a modest radius of 5. The larger this value, the better the far-field approximation of the electrostatic solution is.

The content of the file is given below:

```
#
# a large ball with two smaller balls cut off
#
algebraic3d
solid smallballs = sphere (-1.0, 0.0, 0.0; 0.5)
                    or sphere (1.0, 0.0, 0.0; 0.5);
solid bigball = sphere (0.0, 0.0, 0.0; 5.0);
solid rest = bigball and not smallballs;
tlo rest -col=[0,0,1] -transparent;
```

Open the file and apply the default meshing. In this example two consecutive uniform refinements were performed (choose *Refine Uniform* under *Refinement*) so that the final mesh consisted of 41 693 nodes and 238 976 linear tetrahedrons.

To save the mesh first choose under *File* the *Export Filetype* to be *Elmer*. Then choose *Export Mesh* and save the mesh into a suitable directory to be opened by *ElmerGUI*.

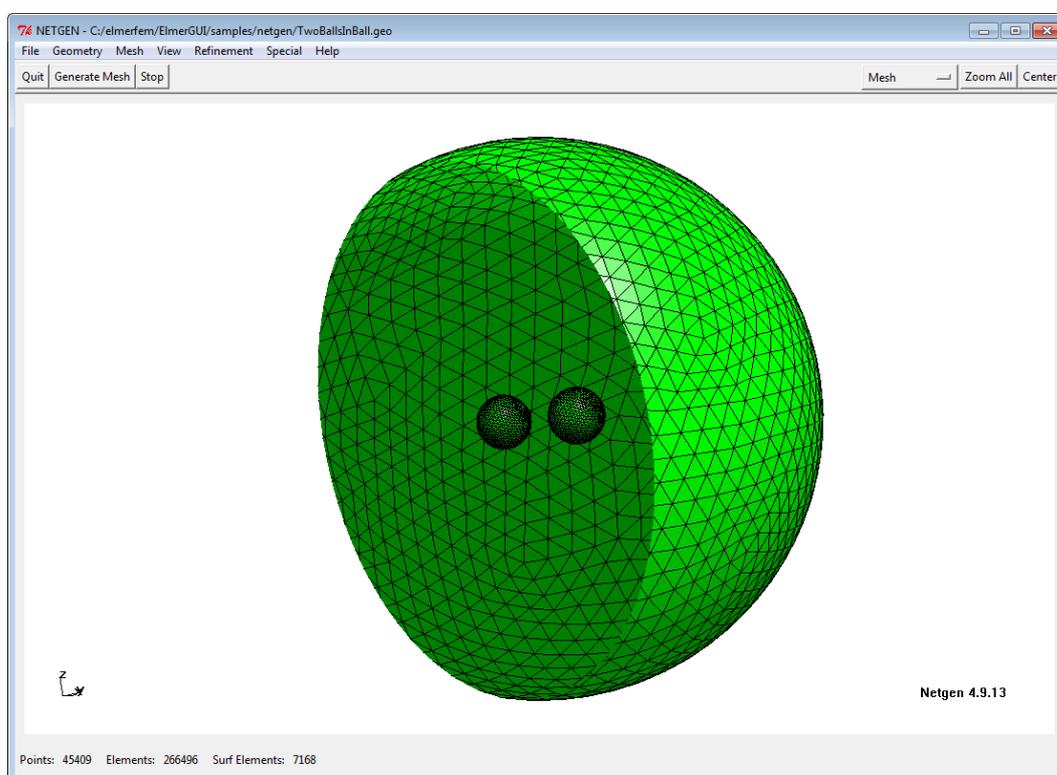


Figure 4.1: Surface mesh for the two inner balls as seen in Netgen

The order of the mesh using nodal elements may be increased by *ElmerGrid*. Assuming the mesh would reside in directory *meshlin* a mesh consisting of quadratic elements may be performed with the following command:

```
ElmerGrid 2 2 meshlin -increase -out meshquad
```

This will maintain the number of elements but the number of nodes will, in this case, increase to 359 009.

### Solution procedure

The definitions for the electrostatic equation may not have been loaded into *ElmerGUI* by default. If this is the case one needs to load these before starting the simulations.

```
File
  Definitions
    Append -> electrostatics.xml
```

The additional definitions should reside in the directory `edf-extra` within the distribution. Moving the desired `xml` files to the `edf`-directory enables automatic loading of the definitions at start-up. By inspecting the definitions in the Elmer Definitions File editor one may inspect that the new definitions were really appended.

The mesh is already created, load it from the directory that was created above.

```
File
  Load Mesh -> mesh
```

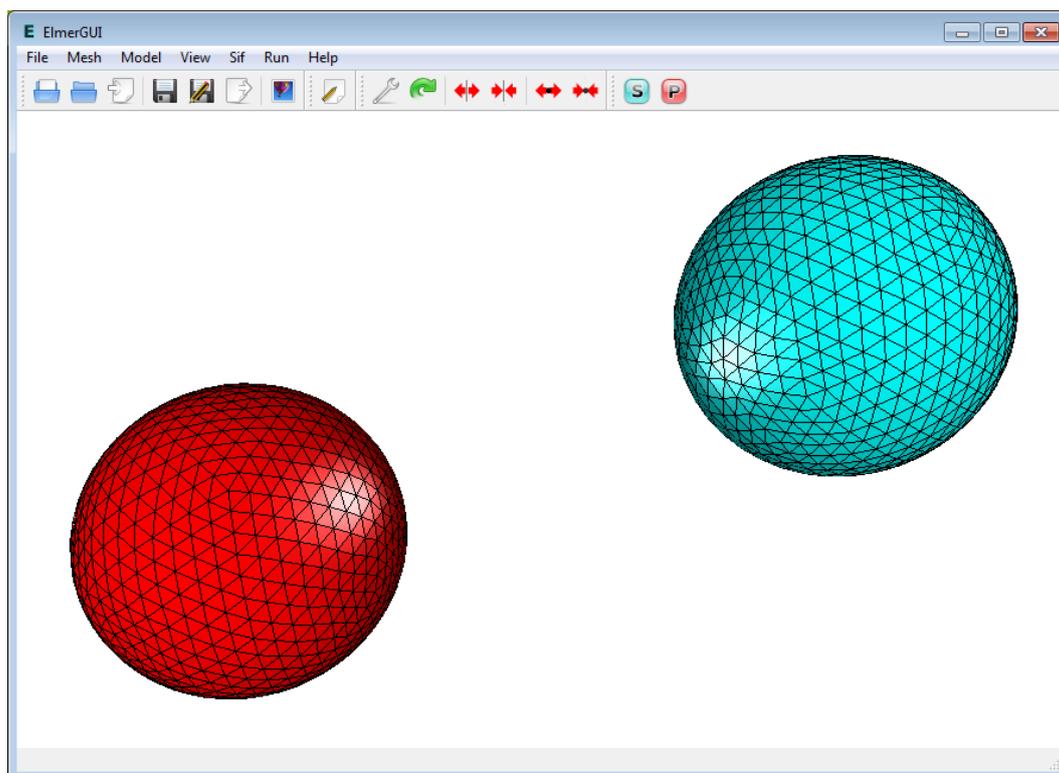


Figure 4.2: The mesh with one highlighted ball as seen in ElmerGUI

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The steady-state simulation is carried out in 3-dimensional cartesian coordinates. For convenience we also set the permittivity of vacuum  $\epsilon_0$  equal to one. This makes it easier to compare the results to the analytical expressions.

```
Model
  Setup
    Simulation Type = Steady state
    Vacuum Permittivity = 1.0
```

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have only the electrostatics solver.

When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore it's easier to assign the Equation and Material to it directly.

In the solver specific options we want to activate some flags that are needed to invoke the computation of derived fields. For the linear system solvers we are happy to use the defaults. One may however, try out different preconditioners (ILU1,...) or direct Umfpack solver, for example.

```
Model
Equation
  Name = Electrostatics
  Apply to Bodies = 1
  Electrostatics
    Active = on
    Edit Solver Settings
      Solver specific options
        Calculate Capacitance Matrix = True
        Calculate Electric Field = True
        Calculate Electric Energy = True
  Add
  OK
```

The Material section includes all the material parameters. In this case we only have the relative permittivity  $\epsilon_r$  which we set to one.

```
Model
Material
  Name = Ideal
  Electrostatics
    Relative Permittivity = 1.0
  Apply to Bodies = 1
  Add
  OK
```

We have two boundary conditions for the potential at the ground and at the capacitor. For other boundaries the do-nothing boundary results to zero flux over the boundary.

```
Model
BoundaryCondition
  Name = Farfield
  Electrostatics
    Electric Infinity BC = True
  Add
  New

  Name = CapBody1
  Electrostatics
    Capacitance Body = 1
  Add
  New

  Name = CapBody2
  Electrostatics
    Capacitance Body = 2
  Add
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

```
Model
```

```
Set boundary properties
  Choose Outer sphere -> set boundary condition Farfield
  Choose one inner sphere -> set boundary condition CapBody1
  Choose the other inner sphere -> set boundary condition CapBody2
```

For the execution ElmerSolver needs the mesh files and the command file. We have know basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```
Sif
  Generate
  Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

```
File
  Save Project
```

After we have successfully saved the files we may start the solver

```
Run
  Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The equation is fully linear and hence only two iterations are needed – the second one just ensures that convergence of the nonlinear level was really obtained. The norm of the solution should be?

When the solution has finished we may start the postprocessor to view some results.

```
Run
  Start postprocessor
```

## Results

The essential result of this case are the values of the capacitance matrix. In this case  $\tilde{C}_{12} \approx 1.691$  and  $\tilde{C}_{10} \approx 5.019$ . For linear elements the obtained figures are 1.6983, 5.0793 and 5.0812, for quadratic Lagrange elements 1.6641, 5.0340 and 5.0340, respectively, and finally for quadratic p-elements 1.6856, 4.9863 and 4.9884.

The values are rather satisfactory with a difference less than 2% from the series approximation.

Note that the derived fields in the StatElecSolver are computed by averaging the fields over elements – not using the Galerkin method which would provide optimal accuracy. To get optimal accuracy, use FluxSolver, for example

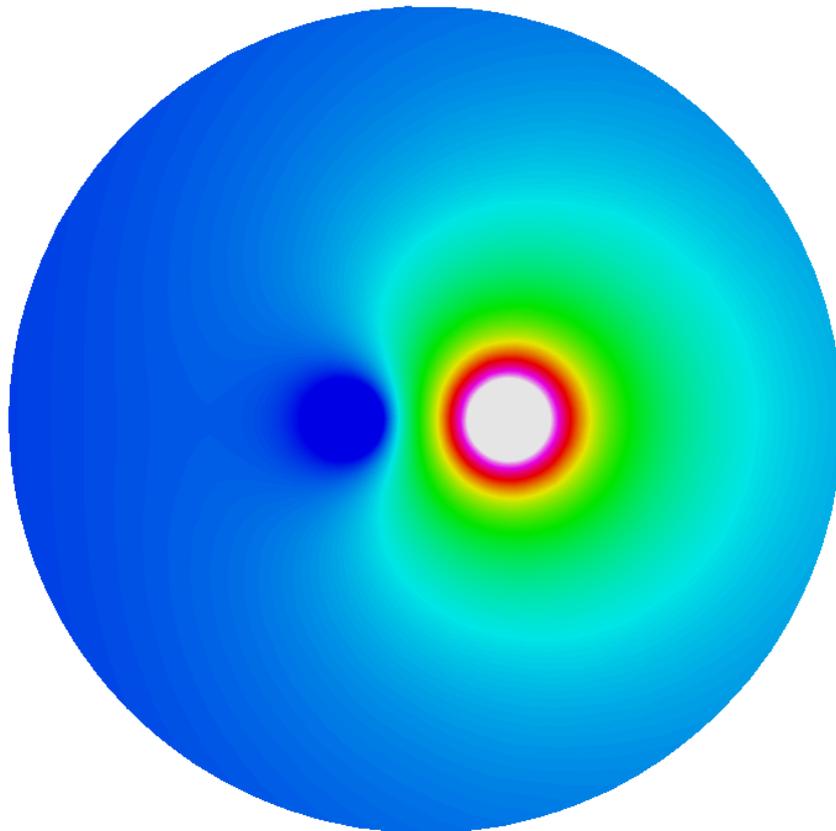


Figure 4.3: The electrostatic potential on the clipping plane. This is the latter of the two symmetric configurations where the unit voltage is applied to one ball and zero voltage to the other, respectively.

## Tutorial 5

# Electrostatic equation – Capacitance of perforated plate

**Directory:** CapacitanceOfPerforatedPlate

**Solvers:** StatElecSolver

**Tools:** ElmerGUI

**Dimensions:** 3D, Steady-state

### Case definition

This case presents solving the Poisson equation for electric potential and calculating appropriate derived quantities, such as capacitance, based on the result. The geometry under study is a perforated plate.

The shape of the holes is assumed to be square with size  $3 \times 3 \text{ mm}^2$ . The holes cover the the other plate uniformly so that the size of each unit cell is  $10 \times 10 \text{ mm}^2$ . The thickness of the plate is assumed to be 1.5 mm and the distance from the reference plate 1.0 mm. The plate may be assumed to be infinitely large. Due to symmetry considerations it suffices to study only one quarter of a unit cell.

The results may be compared to the ideal plate capacitor without holes. For a plane capacitor, the capacitance is

$$C = \varepsilon_r \varepsilon_0 \frac{A}{d}, \quad (5.1)$$

where  $\varepsilon_r$  is the relative permittivity,  $\varepsilon_0$  is the permittivity of vacuum,  $A$  is the area of a capacitor plate,  $d$  is the separation of the capacitor plates, and  $\Phi$  is the potential difference between the plates. For the case under study we get an approximation  $C = 221.36 \text{ fF}$ .

### Preliminaries

The definitions for the electrostatic equation might not have been loaded into ElmerGUI by default. Check the `Model/Equation` menu to verify the situation. If electrostatics is not present one needs to load definitions for it before starting the simulations.

File

Definitions

Append -> electrostatics.xml

The additional definitions should reside in the directory `edf-extra` within the distribution. Moving the desired `xml` files to the `edf`-directory enables automatic loading of the definitions at start-up. By inspecting the definitions in the `Elmer Definitions File` editor one may inspect that the new definitions were really appended.

## Meshing

In this case meshing is performed using ElmerGrid format in file `hexhole.grd` and the ElmerGrid plugin within ElmerGUI. The default mesh is ok and therefore no modifications is needed by the user.

Elmer does not operate an any particular units but usually SI-units are preferred. We therefore choose to scale the problem with 0.001 so that these measurements will be in mm.

Load the mesh file.

File

```
Open -> hexhole.grd
```

You should obtain your mesh and may check that it consists of roughly of 33 159 nodes and of 29 610 linear hexahedral elements.

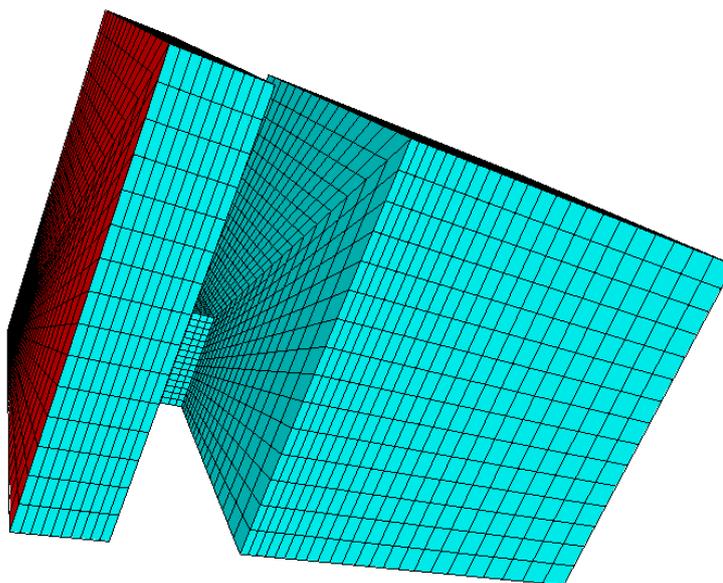


Figure 5.1: The mesh with one highlighted backplate as seen in ElmerGUI

## Case setup

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The steady-state simulation is carried out in 3-dimensional cartesian coordinates. We want to work in mm so we need to scale the mesh with a factor 0.001. There is no direct keyword for that in ElmerGUI but we may use free text input. If you desire to perform visualiazatin with Paraview then you may save the suffix of the Post File to `.vtu`, otherwise ElmerPost or ElmerGUI should be used for visualization.

Model

Setup

```
Simulation Type: Steady state
```

```
Post File: case.vtu
```

```
Free text: Coordinate Scaling = 0.001
```

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have only the electrostatics solver.

When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore it is easier to assign the Equation and Material to it directly.

In the solver specific options we want to activate some flags that are needed to invoke the computation of derived fields. For the linear system solvers we are happy to use the defaults. One may however, try out different preconditioners (ILU1,...) or direct Umfpack solver, for example.

```
Model
  Equation
    Name: Electrostatics
    Apply to Bodies: 1
    Electrostatics
      Active: on
      Edit Solver Settings
        Solver specific options
          Calculate Electric Field: True
          Calculate Electric Energy: True
    Add
  OK
```

The Material section includes all the material parameters. In this case we only have the relative permittivity  $\epsilon_r$  which we could set to one. Alternatively, we can obtain it automatically by choosing the properties of air.

```
Model
  Material
    Add
      Material library
        Air (room temperature)
    Apply to bodies: Body 1
  Add
  OK
```

We have two boundary conditions for the potential at the ground and at the capacitor. For other boundaries the do-nothing boundary results to zero flux over the boundary.

```
Model
  BoundaryCondition
    Name: Ground
    Electrostatics
      Potential: 0.0
  Add
  New

  Name: Capacitor
  Electrostatics
    Potential: 1.0
  Add
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

```
Model
  Set boundary properties
    Choose the backplate -> set boundary condition Ground
    Choose the four pieces of the perforated plate -> set boundary condition Capacitor
```

For the execution ElmerSolver needs the mesh files and the command file. We have know basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```
Sif
  Generate
  Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

```
File
  Save Project
```

After we have successfully saved the files we may start the solver

```
Run
  Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The equation is fully linear and hence only two iterations are needed – the second one just ensures that convergence of the nonlinear level was really obtained. The norm of the solution should be roughly 0.8846.

## Numerical results

The numerical results obtained for capacitance and electric force are compared to those of a complete plane capacitor.

The results of the simulation as well as the comparison to the complete plane capacitor values are shown in Table 5.1.

Table 5.1: Comparison of numerical results to analytic values

relh	C(fF)	ratio
1.0	216.37	0.977
0.7	216.34	
0.5	216.32	

## Visualization

When the solution has finished we may start the postprocessor to view some results. Here we assume that we chose the .vtu format for paraview as output. Then start Paraview.

```
File
  Open: case0001.vtu
  Apply
```

You may now choose the fields to be depicted etc. For more information on the use of of paraview look at the documentation of the software. In figure 5.2 some examples of visualizations with paraview are given.

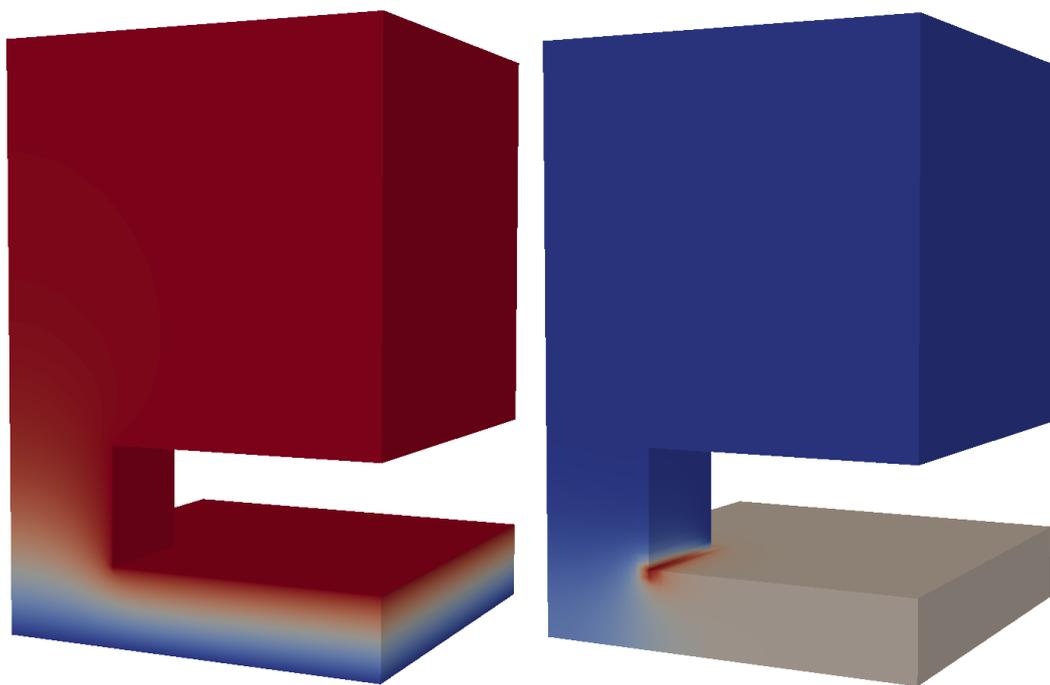


Figure 5.2: The electrostatic potential and the electric energy density of the quarter of a unit cell of a perforated plate capacitor visualized by Paraview.

## Tutorial 6

# Magnetostatics – Magnetic field resulting from a permanent magnet

**Directory:** Horseshoe

**Solvers:** MagnetoDynamics2D

**Tools:** Gmsh, ElmerGUI

**Dimensions:** 2D, Steady-state

### Case definition

This case roughly reproduces the case of a permanent magnet as demonstrated in the following link:

<http://www.strek.strefa.pl/students/meslec/lab06.pdf>

Consider a horseshoe-shaped permanent magnet. It consists of a ferromagnetic material but the two end sections are premagnetized in opposite directions. This results to a familiar magnetic field pattern. The horseshoe consists of three different regions and additionally there is the surrounding air. There is a circular outer boundary in order to conveniently allow for farfield conditions. The material is assumed to have a constant relative permeability of 5000 and the magnetization is set to 750 kA/m.

Note that as this is a 2D case the resulting fields actually are those of an infinitely long horseshoe which of course does not make much sense in real life.

### Meshing

The computational mesh is predefined in Gmsh format in file `horseshoe.msh`. If the user wants to modify the default mesh that must be done with Gmsh. The geometry of the file is given in file `horseshoe.geo`.

### Solution procedure

The definitions for the relevant equation are not loaded into ElmerGUI by default. Hence, one needs to load these before starting the simulations.

File

Definitions

```
Append -> magnetodynamics2d.xml
```

The additional definitions should reside in the directory `edf-extra` within the distribution. Moving the desired `xml` files to the `edf`-directory enables automatic loading of the definitions at start-up. By inspecting the definitions in the Elmer Definitions File editor one may inspect that the new definitions were really appended.

The mesh is already defined, load it from the `samples` directory were it resides.

File

Open -> horseshoe.msh

The ElmerGrid plug-in of ElmerGUI will read the mesh and convert it to a format understood by Elmer.

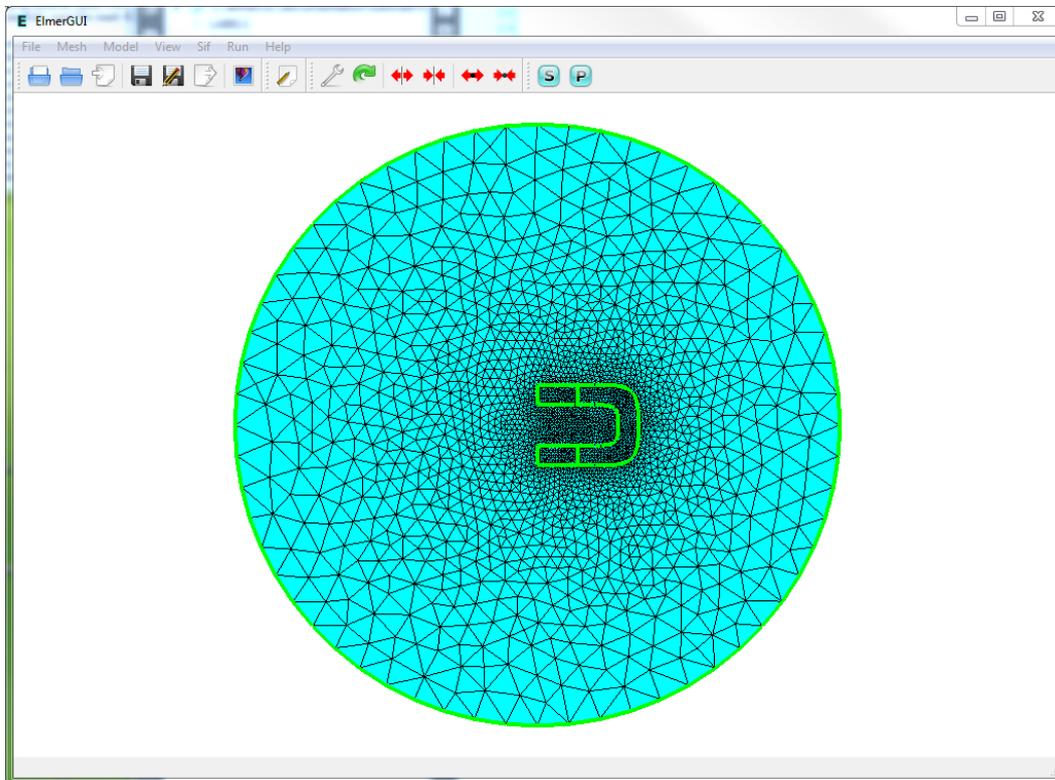


Figure 6.1: The mesh for the horseshoe and surrounding air as seen in ElmerGUI

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The steady-state simulation is carried out in 2-dimensional cartesian coordinates. Nothing needs to be changed here. Currently the permeability of vacuum is not given in the ElmerGUI. To set other than the default value for it, the free text box can be used.

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have the MgDyn2D solver, as well as the postprocessing solver MgDyn2DPost.

When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case the equations need to be solved in all the bodies and hence clicking the all from 1 to 4 here is most convenient. We give a higher priority to the actual solver so that the vector potential will be computed before the derived fields. In this case solver specific options should be ok but they could also be changed in this context.

Model

```
Equation
  Name = MgDyn2D
  Active = on
  Priority = 1
  Apply to Bodies = 1 2 3 4
  Name = MgDyn2DPost
  Active = on
Add
OK
```

The Material section includes all the material parameters. In this case we basically have two different materials but the different magnetization must also be given as a material property. Hence we actually need to define four materials.

```
Model
Material
  Name = Air
  MgDyn2d
    Relative Permeability = 1.0
  Add
  New

  Name = Iron
  MgDyn2d
    Relative Permeability = 5000.0
  Add
  New

  Name = IronPlus
  MgDyn2d
    Relative Permeability = 5000.0
    Magnetization 1 = Real 750.0e3
  Add
  New

  Name = IronMinus
  MgDyn2d
    Relative Permeability = 5000.0
    Magnetization 1 = Real -750.0e3
  Add
  OK
```

We may now assign the material properties by selecting with the mouse. This spares us of the need to know the indexes of each body.

```
Model
Set body properties
  Choose air -> set Material to Air
  Choose curved part of horseshoe -> set Material to Iron
  Choose upper straight part of horseshoe -> set Material to IronPlus
  Choose lower straight part of horseshoe -> set Material to IronMinus
```

We have just one boundary condition i.e. the outer boundary for which we use the farfield condition.

```
Model
BoundaryCondition
  Name = Farfield
  MgDyn2D
    Infinity BC = True
  Add
  OK
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

```
Model
```

Set boundary properties

Choose the 4 pieces of the outer sphere -> set boundary condition Farfield

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

Sif

Generate

Edit -> look how your command file came out

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

File

Save Project

After we have successfully saved the files we may start the solver

Run

Start solver

A convergence view automatically pops up showing relative changes of each iteration. The equation is fully linear and hence only two iterations are needed – the second one just ensures that convergence of the nonlinear level was really obtained. The norm of the solution should be 0.3679.

When the solution has finished we may start the postprocessor to view some results.

Run

Start postprocessor

## Results

The resulting z-component of the vector potential is depicted in Figure 6.2. The corresponding postprocessed magnetic field intensity is depicted in Figure 6.3. Note that the derived fields is enforced to be continuous by default which is not optimal for visualization. For optimal results use Discontinuous Galerkin (DG) method for the postprocessing. Note that when using DG the postprocessing should be done with .vtu files and Paraview. The postprocessing tools of Elmer cannot deal with elementwise-fields.

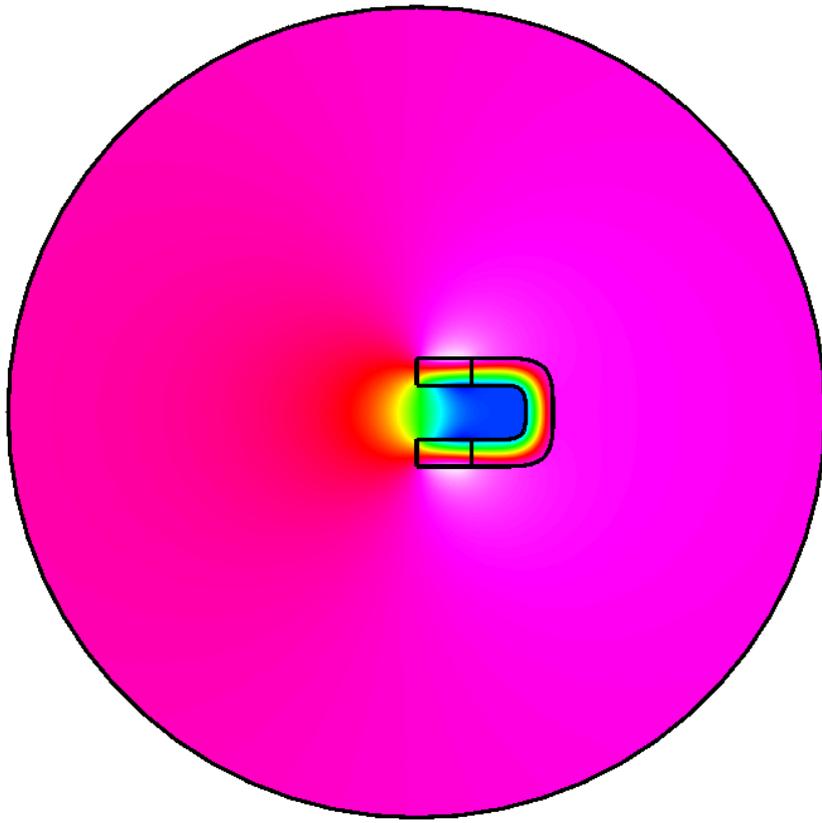


Figure 6.2: The vector potential of the magnetic field.

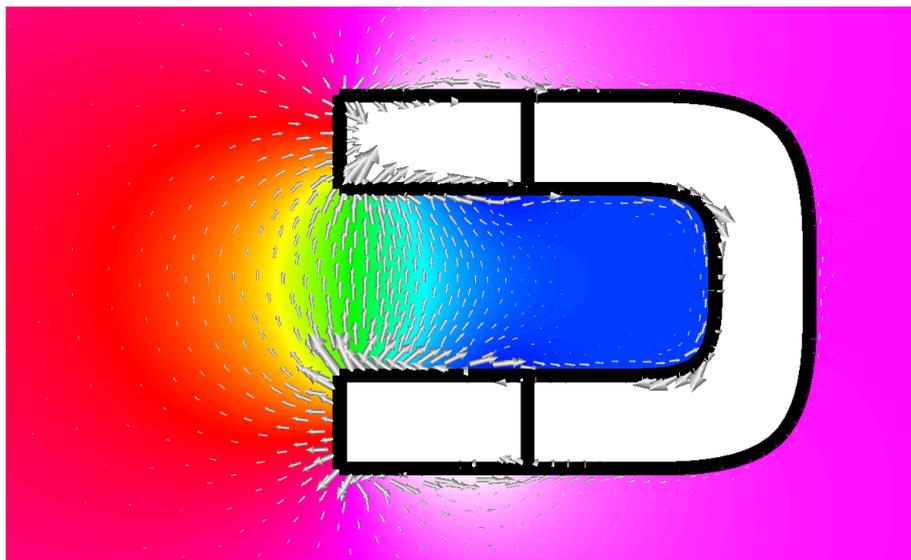


Figure 6.3: A closeup of the vector potential combined with the magnetic field intensity vectors. Note that the fields in the horseshoe itself have been masked away to demonstrate the well known field shape in the free space.

# Tutorial 7

## Harmonic magnetic field in 2D - Induction heating of a graphite crucible

**Directory:** InductionHeatingGUI

**Solvers:** MagnetoDynamics2DHarmonic

**Tools:** Gmsh, ElmerGUI

**Dimensions:** 2D, Axi-Symmetric

### Case definition

At high temperatures the most practical method to heat up the crucible is by electromagnetic induction. The induction coil generates an alternating current that flows through the crucible. The Ohmic resistance encountered by this current dissipates energy, thereby directly heating the crucible via internal heat generation.

The tutorial case is a simple axi-symmetric crucible that could be used, for example, to grow silicon carbide (SiC) with physical vapour deposition. The crucible is made of dense graphite and isolated by porous graphite. At the bottom of the crucible there is some SiC powder. The physical properties of the material are given in Table 7.1. The dimensions of the induction heating crucible are given in Table 7.2.

We neglect the helicity of the coil and assume an average current density that may be computed easily when the area of the coil is known,  $j_0 = nI/A$ , where  $A$  is the coil area. Here we assume a current density of  $1.0\text{e}6 \text{ A/m}^2$ . The frequency of induction heating  $f$  is assumed to be 50 kHz.

The permeability of vacuum is  $4\pi 10^{-7}$  if the other variables are in SI-units. Relative permeability is assumed to be one in all materials.

### Solution procedure

The definitions for the relevant equation are not loaded into ElmerGUI by default. Hence, one needs to load these before starting the simulations.

```
File
  Definitions
    Append -> magnetodynamics2d.xml
```

Table 7.1: Material parameters of the crucible

material	$\varepsilon$	$\kappa$ [W/mk]	$\sigma$ (1/ $\Omega\text{m}$ )
graphite	0.7	10.0	2.0E4
insulation	0.9	1.0	2.0E3
powder	0.5	25.0	1.0E4

Table 7.2: Dimensions of the crucible

body part	$r_{inner}$	$r_{outer}$	$h_{inner}$	$h_{outer}$
graphite	2.0	2.5	6.0	8.0
insulation	2.5	4.0	8.0	12.0
coil	5.0	5.5	8.0	8.0

The additional definitions should reside in the directory `edf-extra` within the distribution. Moving the desired `xml` files to the `edf`-directory enables automatic loading of the definitions at start-up. By inspecting the definitions in the Elmer Definitions File editor one may inspect that the new definitions were really appended.

The mesh is already defined, load it from the `samples` directory were it resides.

File

```
Open -> crucible.msh
```

The ElmerGrid plug-in of ElmerGUI will read the mesh and convert it to a format understood by Elmer.

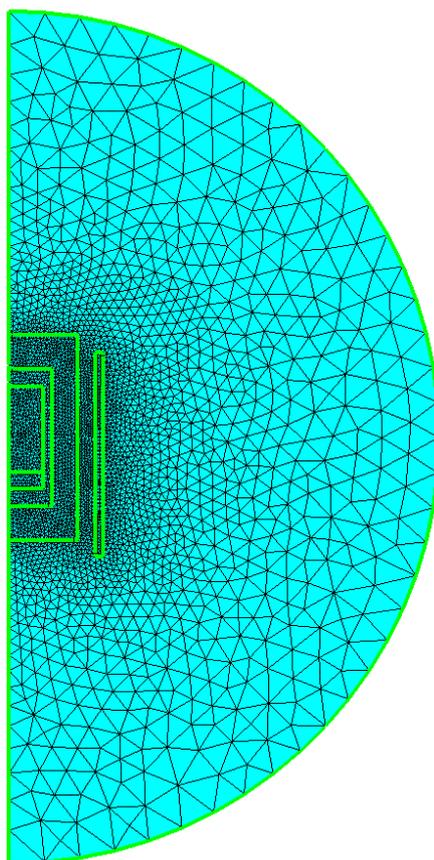


Figure 7.1: The mesh for the horseshoe and surrounding air as seen in ElmerGUI

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. Currently the permeability of vacuum is not given in the ElmerGUI. To set other than the default value for it, the free text box can be used. The steady-state simulation is carried out in rotationally symmetric 2-dimensional

coordinates which must be changed. We also change the post file to have suffix `.vtu` for convenient post-processing with Paraview. If ElmerPost or ElmerGUI is used for visualization the suffix should be `.ep`.

```
Model
  Setup
    Coordinate system -> Axi symmetric
  Post file -> case.vtu
```

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have the MgDyn2DHarmonic solver, as well as the postprocessing solver MgDyn2DPost.

When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case the equations need to be solved in all the bodies and hence clicking the all from 1 to 6 here is most convenient. We give a higher priority to the actual solver so that the vector potential will be computed before the derived fields. In this case solver specific options should be ok but they could also be changed in this context.

```
Model
  Equation
  Solver -> MgDyn2DHarmonic
    Active = on
    Priority = 1
    Angular Frequency = 50.0e3
    Apply to Bodies = 1 2 3 4 5 6
  Solver -> MgDyn2DPost
    Active = on
    Edit Solver Settings
      Solver Specific Options
        Target Variable Complex = on
        Calculate Joule Heating = on
    Name = Induction
  Add
  OK
```

The Material section includes all the material parameters. In this case we basically have two different materials but the different magnetization must also be given as a material property. Hence we actually need to define four materials. The thermal properties are not needed at this stage as we are only solving for the induction. The internal losses of the coil are omitted and it is treated as a pure current source with material properties of air.

```
Model
  Material
    Name = Air
    MgDyn2dHarmonic
      Relative Permeability = 1.0
      Electric Conductivity = 0.0
    Add
    New

    Name = Graphite
    MgDyn2dHarmonic
      Relative Permeability = 1.0
      Electric Conductivity = 2.0e4
    Add
    New

    Name = Insulation
```

```

MgDyn2dHarmonic
  Relative Permeability = 1.0
  Electric Conductivity = 2.0e3
Add
New

Name = Powder
MgDyn2dHarmonic
  Relative Permeability = 1.0
  Electric Conductivity = 1.0e4
Add
New

```

We may now assign the material properties by selecting with the mouse. This spares us of the need to know the indexes of each body.

```

Model
Set body properties
  Choose external air -> set Material to Air
  Choose coil -> set Material to Air
  Choose insulation (outermost body) -> set Material to Insulation
  Choose graphite (actual crucible) -> set Material to Graphite
  Choose powder at the bottom of crucible -> set Material to Powder
  Choose internal air above the powder-> set Material to Air

```

We need to provide a current source in order for the equation to have a nontrivial solution.

```

Model
BodyForce
  Name = CurrentSource
MgDyn2DHarmonic
  Current Density = 2.5e5
Add
OK

```

This must be also jointed with the coil

```

Model
Set body properties
  Choose coil -> set Body force to CurrentSource

```

We have just one boundary condition i.e. the outer boundary for which we use the farfield condition.

```

Model
BoundaryCondition
  Name = Farfield
MgDyn2DHarmonic
  Infinity BC = True
Add
OK

```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

```

Model
Set boundary properties
  Choose the 2 pieces of the exterior -> set boundary condition Farfield

```

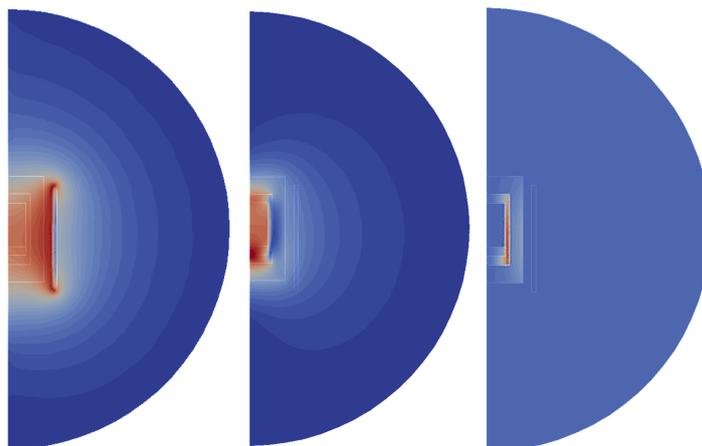


Figure 7.2: Induction heating of a simple crucible. a) in-phase component of the magnetic field intensity b) out-of-phase component of the magnetic field intensity c) Joule losses in the conductors

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```
Sif
  Generate
  Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

```
File
  Save Project
```

After we have successfully saved the files we may start the solver

```
Run
  Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The equation is fully linear and hence only two iterations are needed – the second one just ensures that convergence of the nonlinear level was really obtained. The norm of the solution should be 0.3679.

When the solution has finished we may start the postprocessor to view some results.

```
Run
  Start postprocessor
```

With the given computational mesh the problem is solved in a few seconds. With the 6 542 linear triangles the heating efficiency is estimated to be 18.9 W. The corresponding results are shown in Fig. 7.2.

It can be noted that would the estimated heating efficiency be different from the known one the user may give the postprocessing solver the `Desired Heating Power` in order to scale the potential of the solution. The solution, on the other hand, may be used as a source term in heat equation, for example.

## Tutorial 8

# Navier-Stokes equation – Laminar incompressible flow passing a step

**Directory:** FlowStepGUI

**Solvers:** FlowSolve

**Tools:** ElmerGUI

**Dimensions:** 2D, Steady-state

### Case definition

This tutorial represents the canonical step flow of viscous fluid. A fluid, flowing past a step (see figure 8.1), has the density 1 kg/m and viscosity 0.01 kg/ms. The velocity profile at the inlet is parabolic with a mean velocity  $\langle v_x \rangle = 1.0$  m/s and  $v_y = 0.0$  m/s. At the outlet only the vertical component is defined,  $v_y = 0.0$  m/s. At all other walls the no-slip boundary condition,  $\vec{v} = 0$ , is applied. Thus the Reynolds number for the case is around 100.

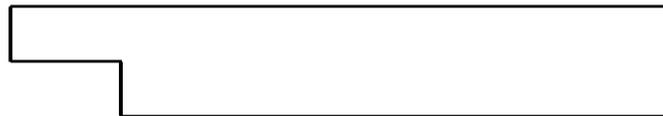


Figure 8.1: Geometry of the step flow problem

Mathematically the problem to be solved is

$$\begin{cases} -\nabla \cdot (2\mu\bar{\varepsilon}) + \rho\vec{u} \cdot \nabla\vec{u} + \nabla p = 0 & \text{in } \Omega \\ \nabla \cdot \vec{u} = 0 & \text{in } \Omega \end{cases} \quad (8.1)$$

with the boundary conditions

$$\begin{cases} u_x = 1 & \text{on } \Gamma_{inlet} \\ u_x = 0 & \text{on } \Gamma_{no-slip} \\ u_y = 0 & \text{on } \Gamma_{inlet} \cup \Gamma_{outlet} \cup \Gamma_{no-slip} \end{cases} \quad (8.2)$$

where  $\mu$  is the viscosity,  $\bar{\varepsilon}$  is the strain tensor,  $\rho$  is the density,  $\vec{u}$  is the velocity and  $p$  is the pressure. It is assumed that the density and viscosity are constants.

## Solution procedure

The mesh is given in ElmerGrid format in file `step.grd`, load this file.

File

```
Open -> step.grd
```

You should obtain your mesh and may check that it consists of 9696 nodes and of 9442 bilinear elements.

Model

```
Summary...
```

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation. The steady-state simulation is carried out in 2-dimensional cartesian coordinates, which are also the defaults.

Model

```
Setup
```

```
Simulation Type = Steady state  
Coordinate system = Cartesian
```

In the equation section we choose the relevant equations and parameters related to their solution. In this case the only the Navier-Stokes equation is needed.

When defining Equations and Materials it is possible to assign the to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore its easier to assign the Equation and Material to it directly. One could also edit the solver setting in order to try different strategies for solving the nonlinear or linear system. Initially the Navier-Stokes solver uses the more robust Picard iteration which is changed to Newton iteration after few initial steps. For the given viscosity the default values are ok, but may need tuning when going into higher Reynolds numbers.

Model

```
Equation
```

```
Name = Navier-Stokes  
Apply to Bodies = Body 1  
Navier-Stokes  
Active = on  
Edit Solver Setting  
Nonlinear System  
Max. iterations = 20  
Newton after iterations = 3
```

```
Add  
OK
```

The Material section includes all the material parameters. They are divided to generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the density. Other properties assume a physical law, such as viscosity.

Model

```
Material
```

```
Name = Ideal  
General  
Density = 1.0  
Navier-Stokes  
Viscosity = 0.01  
Apply to Bodies = Body 1  
Add  
OK
```

The current case does not have any body forces. Convergence should also be obtained using the default initial condition which sets all field values to zero. Hence no setting for initial condition are needed.

Only one boundary condition may be applied to each boundary and therefore all the different physical BCs for a boundary should be grouped together. In this case the Temperature and Velocity. The side walls are assumed to be adiabatic.

The parabolic inlet-profile is achieved using the MATC environment. To be able to edit the content of the inlet profile click `Enter` to open an edit box for the `Velocity 1`. The given expression will be interpreted at run-time so that  $v_x = 6(y - 1)(2 - y)$ . As  $y \in [1, 2]$  thereby creating a parabolic velocity profile with a mean velocity of unity.

Model

```
BoundaryCondition
  Name = Inlet
  Navier-Stokes
    Velocity 1 = Variable Coordinate 2; Real MATC "6*(tx-1)*(2-tx)"
    Velocity 2 = 0.0
  Add
  New

  Name = Outlet
  Navier-Stokes
    Velocity 2 = 0.0
  Add
  New

  Name = Walls
  Navier-Stokes
    Noslip wall BC = on
  Add
  OK
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

Model

```
Set boundary properties
  Choose Inlet -> set boundary condition Inlet
  Choose Outlet -> set boundary condition Outlet
  Choose Walls -> set boundary condition Walls
```

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

Sif

```
Generate
Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case. Create a suitable directory for the case if needed.

File

```
Save Project
```

After we have successfully saved the files we may start the solver

Run

```
Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The problem should converge in about ten iterations to a norm of 0.4347 visible on the output.

When there are some results to view we may start the postprocessor also

Run

```
Start postprocessor
```

## Results

The results may be viewed using the postprocessor as shown in Figure 8.2 and 8.3. One may also register specific values, for example the pressure difference is 0.388 Pa, the minimum and maximum lateral velocities are -0.1666 m/s and 1.5 m/s, respectively. One special result of interest is the point, on the x-axis, at which the direction of the flow changes. In this case its position is about 5.0 m after the step.

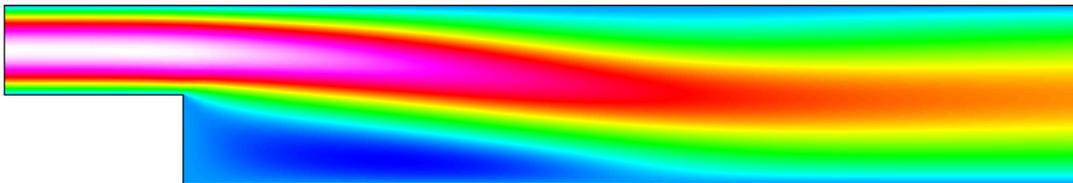


Figure 8.2: Absolute value of the velocity field



Figure 8.3: Pressure field

### Extra task: Decreasing the viscosity

Try what happens if the viscosity is further decreased by a factor 10. Convergence may be difficult to obtain. Some tricks that may be tested include

- Introducing a relaxation factor (typically in the range 0.5–0.7)
- Increasing number of nonlinear iterations
- Favoring Picard iteration over Newton
- Increasing mesh density (and length of domain)

Don't be worried if you fail to find convergence. This task will mainly act as a motivator in using turbulence models for higher Reynolds numbers.

Remember to re-perform the following phases in order to get the updated results

```
Sif
  Generate
File
  Save Project
Run
  Start solver
```

You may just reload the results in the postprocessor rather than closing and opening the program.

# Tutorial 9

## Vortex shedding – von Karman instability

**Directory:** VonKarmanGUI

**Solvers:** FlowSolve

**Tools:** ElmerGUI

**Dimensions:** 2D, Transient

### Case definition

This tutorial is about simulating the developing of the vortex shedding i.e. the von Karman instability. The geometry is a tube with a circular obstacle. For more details on the problem look at the benchmark case definition by M. Schäfer and S. Turek in "*Benchmark computations of laminar flow around a cylinder*".

### Solution procedure

The mesh is given in 2d netgen format in file `circle_in_channel.in2d`, load this file.

File

```
Open -> circle_in_channel.in2d
```

You should get a mesh consisting of 749 nodes and 1328 triangles. This is a rather sparse mesh. To increase the element number

Mesh

Configure

```
nlib / Max H: 0.02
```

Mesh

Remesh

This mesh includes 3464 nodes and 6506 triangles. The mesh is presented in figure 9.1.

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 2-dimensional cartesian coordinates. 2nd order bdf time-stepping method is selected with 200 steps and we want the total simulation time to be 8 seconds.

Model

Setup

```
Simulation Type = Transient
```

```
Steady state max. iter = 1
```

```
Time Stepping Method = bdf
```

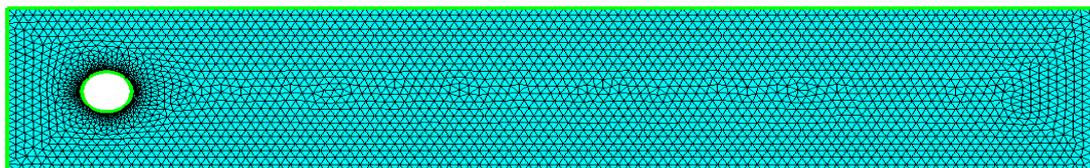


Figure 9.1: Computational mesh of the problem.

```
BDF Order = 2
Time Step Intervals = 200
Time Step Sizes = $ 8/200
```

For the solver specific settings we are quite happy to use the defaults. However, we relax a little bit the convergence tolerances to get speedier simulation.

```
Model
Equation
  Name = Navier-Stokes
  Apply to Bodies = 1
  Navier-Stokes
    Active = on
  Edit Solver Settings
    Nonlinear system
      Convergence tol. = 1.0e-4
    Linear System
      Convergence tol. = 1.0e-6
  Add
  OK
```

The Material section includes all the material parameters. Here we choose simple parameters for the academic test case

```
Model
Material
  Name = Ideal
  General
    Density = 1
  Navier Stokes
    Viscosity = 0.001
  Apply to Bodies = 1
  Add
  OK
```

The system does not need any body forces nor initial conditions i.e. we are happy with the default guess zero.

We have three different kinds of boundaries: inlet, no-slip walls, and outlet. The inlet has a parabolic fully developed laminar profile with a maximum velocity of 1.5 m/s. Additionally for the inlet the vertical velocity component is assumed zero. The circle and the lower and upper walls are given the no-slip treatment.

For the outlet only the vertical component is set to zero since the default discretization weakly imposes a zero pressure condition if the normal velocity component is not defined.

Model

```
BoundaryCondition
  Name = Inlet
  Navier-Stokes
    Velocity 1 = Variable Coordinate 2; Real MATC "4*1.5*tx*(0.41-tx)/0.41^2"
    Velocity 2 = 0.0
  Add
  New

  Name = Walls
  Navier-Stokes
    Velocity 1 = 0.0
    Velocity 2 = 0.0
  Add
  New

  Name = Outlet
  Navier-Stokes
    Velocity 2 = 0.0
  Add
  Ok
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

Model

```
Set boundary properties
  Choose inlet -> set boundary condition Inlet
  Choose both horizontal walls and circle -> set boundary condition Walls
  Choose outlet -> set boundary condition Outlet
```

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

Sif

```
Generate
Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

File

```
Save Project
```

After we have successfully saved the files we may start the solver

Run

```
Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The norm after the first timestep should be around 0.695, and after last 0.749, respectively.

When there are some results to view we may start the postprocessor also

Run

```
Start postprocessor
```

## Results

Due to the number of the time-steps the simulation will take a few minutes. You may inspect the results with ElmerPost as the time-steps are computed, or wait until all timesteps have been computed. When opening the result file using ElmerGUI ElmerPost only opens the first time-step. Therefore it is important to reopen the file and load the time-steps of interest. Pressing the button `All` selects all the calculated time steps. A video of the results can be viewed by selecting the option `Timestep Control` and pressing the button `Loop` under the `Edit` menu.

In Figure 9.2 the velocity field is presented for three different timesteps. The maximum velocity in the system should be about 2.1724 m/s.

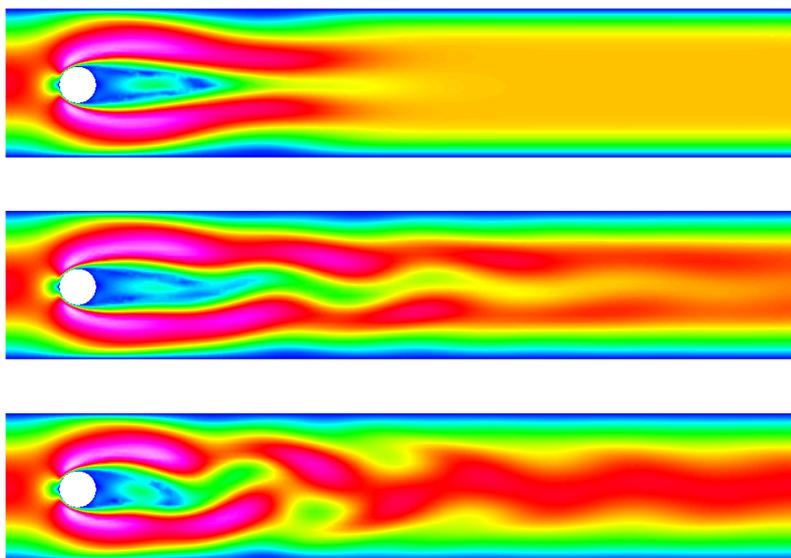


Figure 9.2: Temperature distribution at steps 20, 100 and 200

## Effect of Reynolds number

The Reynolds number in this case is around 100 resulting to unsteady flow. The critical Reynolds number is around 90 and reducing the flow velocity so that Reynolds number becomes, say 20, makes the system to possess a steady-state solution. On the other hand, increasing the velocity will make the von Karman vortices even more pronounced until they break into fully chaotic motion. This finite element mesh will allow only minor increase in Reynolds number to be able to capture the phenomena.

# Tutorial 10

## Thermal flow in curved pipe

**Directory:** CurvedPipeGUI

**Solvers:** HeatSolve, FlowSolve

**Tools:** ElmerGUI

**Dimensions:** 3D, Steady-state

### Case definition

This tutorial demonstrates how to set up a coupled case of thermal flow in curved pipe with a finite thickness. Within the pipe both the flow and heat transfer equations need to be solved while on the solid section only heat transfer needs to be considered.

The inner diameter of the pipe is 0.01 m and the outer 0.012 m, respectively. It is bend to a 135 degree angle with a radius of 0.02 m. Beyond the bend 0.03 m of the direct part is also accounted for. The fluid flowing in the pipe is water with an original temperature of 350 K. The outer temperature of the iron pipe is 300 K making the water gradually to cool.

The water is injected with a parabolic velocity profile with a maximum of 0.01 m/s. In reality the laminar analytic profile is described by the Bessel's function. Here the flow is treated as laminar and steady-state even though at these Reynolds number 100 the unsteady nature of the flow should probably be considered. This would enhance the heat transfer. The steady-state case, however, will achieve the educational goals of the tutorial.

### Solution procedure

The mesh is defined in ElmerGrid format in file `curved_pipe.grd`, load this file.

File

```
Open -> curved_pipe.grd
```

You should obtain your mesh and may check that it consists of 23670 trilinear bricks and 25245 nodes. The density of the mesh may be varied by altering the `Reference Density` in the file. For further information on the mesh definition look at the `ElmerGrid` manual. Often it is desirable to use some professional mesh generation tool in CFD and translate it into Elmer format. For educational purposes we are quite happy to use this simple geometry.

After we have the mesh we start to go through the `Model` menu from the top to bottom. In the `Setup` we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 3-dimensional cartesian coordinates in steady-state. There is nothing really to be done here, but you may verify that the defaults are correct.

Model

```
Setup
```

```
Coordinate system = Cartesian
```

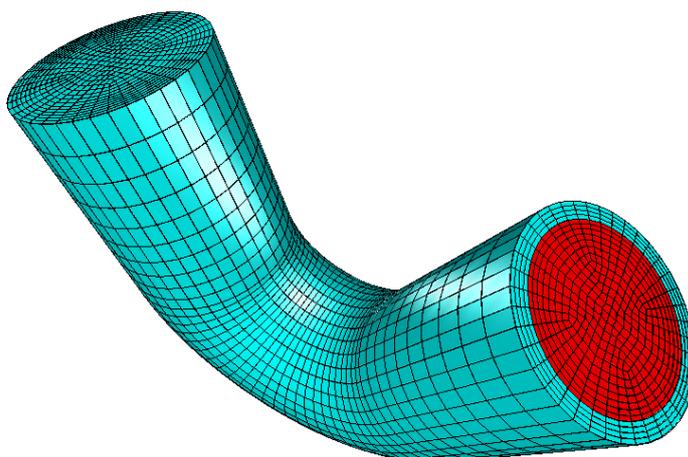


Figure 10.1: The mesh of the curved pipe as seen in ElmerGUI

```
Simulation type = Steady state
Steady state max. iter = 1
...
```

In the Equation section we choose the relevant equations and parameters related to their solution. In this case we'll have two different sets of solvers (called as Equation in Elmer slang). The other consists of heat and flow solvers, while the other includes just the heat solver. We'll name them appropriately.

When defining Equations and Materials it is possible to assign them to bodies immediately, or to use mouse selection to assign them later. In this case we know that the fluid body has the index 1 and the solid body has the index 2. Therefore it is easy to assign the Equation and Material to the bodies directly.

Here we neglect the effect of natural convection. Therefore there is just one-directional coupling from the flow to heat transfer. In order to follow the direction of causality we address the flow solver with a higher priority than the heat solver (default is zero).

Here we are quite happy with the default solver settings of the individual equations. However, for the flow solver we change the default preconditioner ILU0 to ILU1 to enhance convergence (with increased memory consumption). For 3D cases the direct solvers are usually not feasible so it is better to stick with the iterative BiCGstab linear solver.

The equation for the fluid

```
Model
Equation
Add
Name = Heat and Flow
Apply to Bodies = 1
Heat Equation
Active = on
Convection = Computed
Navier-Stokes
Active = on
Priority = 1
Edit Solver Setting
Linear System
Preconditioning = ILU1
OK
```

and then for the solid

```

Model
  Equation
    Add
    Name = Just Heat
    Apply to Bodies = 2
    Heat Equation
      Active = on
      Convection = None
    OK

```

The Material section includes all the material parameters. They are divided into generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the density. Other properties assume a physical law, such as conductivities and viscosity.

Here we choose water and iron from the material library. You may click through the material parameters of the various solvers to ensure that the properties are indeed as they should be. Any constant set of units may be used in Elmer. The natural choice is of course to perform the computations in SI units.

```

Model
  Material
    Add
    Material library
      Water (room temperature)
    Apply to Bodies = 1
    OK

    Add
    Material library
      Iron (generic)
    Apply to Bodies = 2
    OK

```

The Body force section usually represents the right-hand-side of an equation. It could be used to account for the natural convection, for example. In this case, however, we do not apply any body forces.

Also an Initial condition could be given in steady-state case to enhance convergence. However, in this case convergence is pretty robust with the default guess of zero.

We have four different boundary conditions: thermal inflow, internal no-slip, outflow, and external fixed temperature. Otherwise natural BCs are assumed. As it is tedious to know the indexes by heart we first define the different BCs and only afterwards apply them to the existing boundaries with the mouse.

```

Model
  BoundaryCondition
    Name = HotInflow
    Heat Equation
      Temperature = 350.0
    Navier-Stokes
      Velocity 1 = 0.0
      Velocity 2 = 0.0
      Velocity 3 = Variable Coordinate
      Real MATC "100.0*(1.0e-4-tx(0)^2-tx(1)^2)"
    Add
    New

```

The condition for Velocity 3 above may easiest be typed by pressing Enter-key in the edit box which will open a larger window for editing.

```
Name = Outflow
```

```

Navier-Stokes
  Use normal-tangential coordinate system = on
  Velocity 2 = 0.0
  Velocity 3 = 0.0

```

```
Add
```

```
New
```

```

Name = NoSlip
Navier-Stokes
  NoSlip Wall BC = on

```

```
Add
```

```
New
```

```

Name = Troom
Heat Equation
  Temperature = 300.0

```

```
Add
```

When choosing the boundaries it is important that you choose the right inlet. For that purpose you may activate the compass,

```

View
  Compass = on

```

Now the inlet is the one with normal pointing at the  $z$ -direction. Now we are ready to choose the boundaries

```

Model
  Set boundary properties
    Choose inlet face -> set boundary condition HotInflow
    Choose outlet face -> set boundary condition Outflow
    Choose outer side -> set boundary condition Troom

```

Unfortunately we cannot see the internal boundary. For that purpose click on the outer boundary and choose

```

View
  Hide/show selected

```

The outer boundary should vanish and you can proceed with the last BC,

```

Model
  Set boundary properties
    Choose internal side -> set boundary condition Noslip

```

For the execution ElmerSolver needs the mesh files and the command file. We have know basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

```

Sif
  Generate
  Edit -> look how your command file came out

```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case. It's a good idea to give the project an illuminating name. Avoid paths which includes empty spaces since they may cause problems later on.

```

File
  Save Project
  Make New Folder -> curved_pipe
  OK

```

After we have successfully saved the files we may start the solver

```
Run
Start solver
```

A convergence view automatically pops up showing relative changes of each iteration. The simulation may take a few minutes depending on your platform. After the simulation has terminated we may study the results.

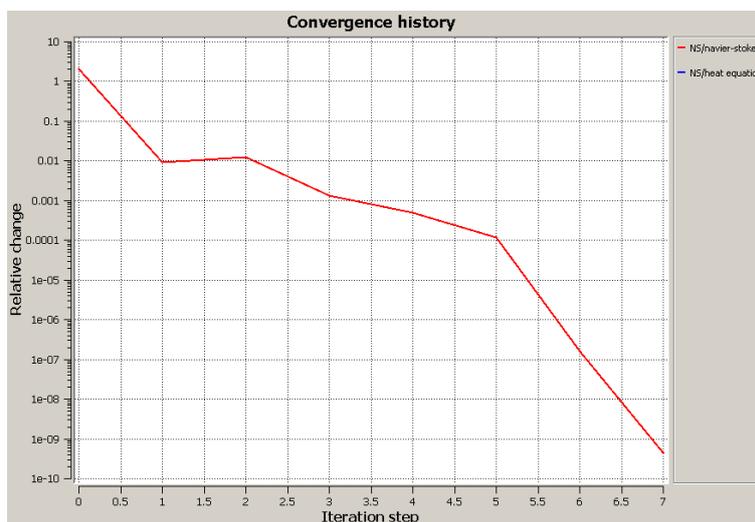


Figure 10.2: Convergence history of the case

## Results

The computed norms should be 3.255 for the Navier-Stokes equation and 324.66 for the heat equation. If there is some discrepancy the setup of the system was probably different from the one in the tutorial.

To visualize the results open the postprocessor, in this case `ElmerPost`. After the simulation has terminated we may open the postprocessor to view the results.

```
Run
Start postprocessor
```

A standard way of visualizing is to choose `ColorMesh` and there choose `Surface` and the desired field variable, for example `Velocity_abs` or `Temperature`. In this case only the outflow crosssection contains any information. It may be seen in Figure 10.3 that the symmetry around pipe origin is lost in the bent.

Alternatively we may visualize the crosssection at  $y = 0$ . To that aim choose `Isocontours` and there set the `Number Of Isosurfaces` to 1, choose `Surface`, set `Contour Variable` to `nodes_y`, and `Color Variable` to `Temperature` etc. Now you may nicely see how the velocity profile affects the temperature distribution in the pipe.

In Figures 10.5 and 10.4 the obtained velocity and temperature distributions are presented.

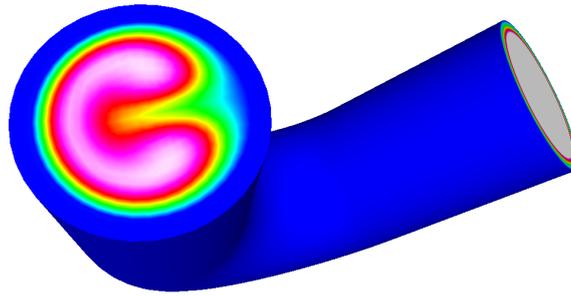
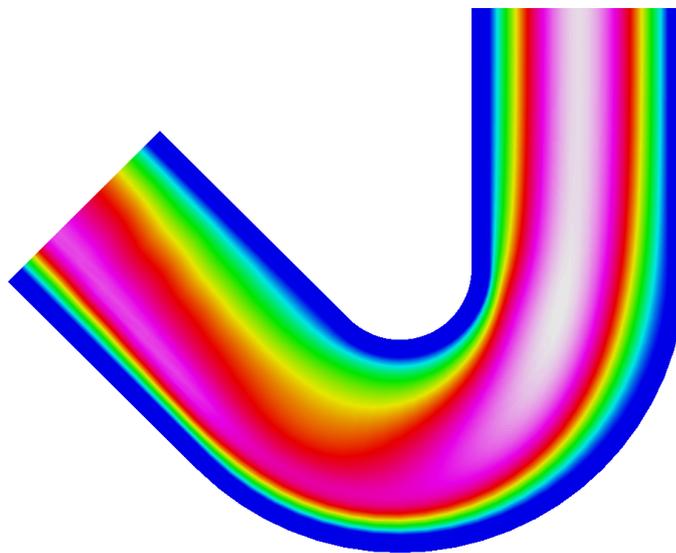
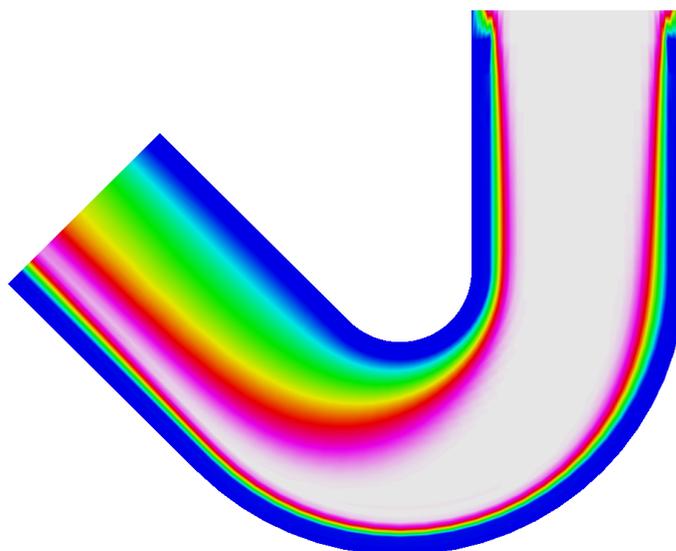


Figure 10.3: Temperature distribution at the outlet of the pipe

Figure 10.4: Velocity distribution at the cross section  $y = 0$ .Figure 10.5: Temperature distribution at the cross section  $y = 0$ .

# Tutorial 11

## Interaction between fluid flow and elastic obstacle

**Directory:** FsiObstacleGUI

**Solvers:** FlowSolve,ElasticSolve,MeshSolve

**Tools:** ElmerGUI

**Dimensions:** 2D, Steady-state

### Case definition

This tutorial demonstrates how to set up a coupled case of fluid-structure interaction. Flow initiated at one end of a channel which has an elastic obstacle that bends under the influence of fluidic forces. The resulting displacement modify the domain thereby affecting the flow of the fluid.

The channel is assumed to be 2D. The length of the is 10 m and the height is 2 m. At 2 m sits a elastic beam with a rounded top the height of which is 1.2 m and width 0.4 m. A parabolic velocity profile with maximum velocity of 1 m/s is assumed.

Material properties are assumed to be rather simple: For the structure density is  $1000 \text{ kg/m}^3$ , Youngs module is  $1000 \text{ Pa}$ , and Poisson ratio 0.3. For the fluid the density is  $1 \text{ kg/m}^3$  and viscosity is  $0.1 \text{ Pas}$ . Additionally the fluid has elastic properties that are used to extent the displacement of the elastic beam to the fluid.

The idea of the case definition is to demonstrate simple yet strongly coupled FSI case without getting into turbulence modeling. Realistic material parameters in the given size of the domain would easily result to turbulence and just small displacements.

The case is solved using standard weak coupling with some relaxation to boost the convergence. The solution is steady-state so only the final results are will be studied.

of thermal flow in curved pipe with a finite thickness. Within the pipe both the flow and heat transfer equations need to be solved while on the solid section only heat transfer needs to be considered.

### Solution procedure

The nonlinear elasticity equation is not by default activated in the menu structures ElmerGUI. Hence, the user must load these before starting the simulations.

File

Definitions

Append -> nonlinearelasticity.xml

The additional definitions should reside in the directory `edf-extra` within the distribution. Moving the desired `xml` files to the `edf`-directory enables automatic loading of the definitions at start-up. By inspecting

the definitions in the Elmer Definitions File editor one may inspect that the new definitions were really appended.

The mesh is defined in .in2d format, the 2D format of netgen, in file `obstacle_in_channel.in2d`, load this file.

File

```
Open -> obstacle_in_channel.in2d
```

The default mesh is obviously too sparse. To make the mesh more dense set

```
Mesh -> Configure -> nglib -> Max H: 0.1
```

and choose

```
Mesh -> Remesh
```

You should obtain a denser mesh and may check that it consists of around 4140 nodes and 7890 linear triangles.

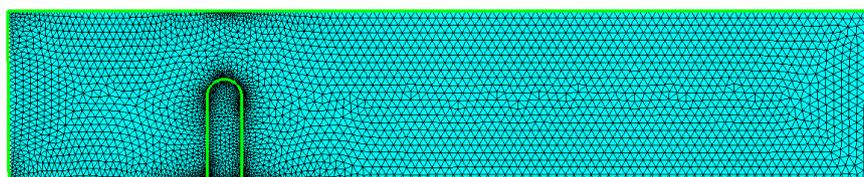


Figure 11.1: The mesh of the obstacle in channel case as seen in ElmerGUI

After we have the mesh we start to go through the `Model` menu from the top to bottom. In the `Setup` we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 2-dimensional cartesian coordinates in steady-state. There is not much to do here, just increase the number of iterations needed for the convergence of the coupled system. We also set the output interval to zero which means that results are written only at the end of the case.

Model

Setup

```
Coordinate system = Cartesian
Simulation type = Steady state
Steady state max. iter = 100
Output Intervals = 0
...
```

In the `Equation` section we choose the relevant equations and parameters related to their solution. In this case we'll have two different sets of solvers (called as `Equation` in Elmer slang). The fluid domain consists of flow and mesh deformation solvers, while the elastic domain just includes the nonlinear elasticity solver. We'll name them appropriately.

To enhance the convergence and efficient use of resources we set relaxation factors of the primary solvers to 0.5 and the number of nonlinear iterations to 1. The mesh deformation solver just extends the displacements of the elasticity solver to the fluid domain, so no relaxation is needed here. For the linear systems we are quite happy with the defaults.

To honor the causality the flow solver should be solved first, then the elasticity solver and as last the mesh deformation solver. We set the priorities accordingly. The equation for the fluid flow + mesh deformation

Model

```
Equation
```

```

Add
Name = Flow and mesh deform
Apply to Bodies = 1
Navier-Stokes
  Active = on
  Priority = 2
  Edit Solver Setting
    Nonlinear System
      Max.iterations = 1
      Nonlinear System Relaxation Factor = 0.5
Mesh Update
  Active = on
  Priority = 0
OK

```

and then for the solid

```

Model
Equation
Add
Name = Elasticity
Apply to Bodies = 2
Nonlinear Elasticity
  Active = on
  Priority = 1
  Edit Solver Setting
    Nonlinear System
      Max.iterations = 1
      Nonlinear System Relaxation Factor = 0.5
OK

```

Next we set our rather simple material parameters. The Material section includes all the material parameters. They are divided into generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the density. Other properties assume a physical law, such as conductivities and viscosity.

```

Model
Material
Add
Name = Ideal fluid
General
  Density = 1.0
Navier-Stokes
  Viscosity = 0.1
Mesh Update
  Elastic Modulus = 1.0
  Poisson Ratio = 0.3
Apply to Bodies = 1
OK

Add
Name = Ideal structure
General
  Density = 1.0e3
Nonlinear Elasticity
  Youngs Modulus = 1.0e3

```

```

Poisson Ratio = 0.3
Apply to Bodies = 2
OK

```

The `Body force` section usually represents the right-hand-side of an equation. In this case we do not need any body forces.

Also an `Initial condition` could be given in steady-state case to enhance convergence. However, in this case convergence is pretty robust with the default guess of zero.

We have five different boundary conditions: inflow, outflow, lateral walls with no-slip conditions, fsi conditions, and the beam base. As it is tedious to know the indexes by heart we first define the different BCs and only afterwards apply them to the existing boundaries with the mouse.

```

Model
BoundaryCondition
  Name = Inflow
  Navier-Stokes
    Velocity 1 = Variable Coordinate 2
    Real MATC "tx*(2-tx)"
    Velocity 2 = 0.0
    Mesh Update 1 = 0.0
  Add
  New

```

The condition for `Velocity 1` above may easiest be typed by pressing `Enter`-key in the edit box which will open a larger window for editing.

```

Name = Outflow
Navier-Stokes
  Velocity 2 = 0.0
Mesh Update
  Mesh Update 1 = 0.0
Add
New

```

```

Name = Walls
Navier-Stokes
  NoSlip Wall BC = on
Mesh Update
  Mesh Update 1 = 0.0
  Mesh Update 2 = 0.0
Add
New

```

```

Name = Base
Nonlinear Elasticity
  Displacement 1 = 0.0
  Displacement 2 = 0.0
Add
New

```

The essence of fluid-structure interaction is in the following boundary condition. When the `Fsi BC` is active the fluidic forces are automatically within `ElasticSolver`. The backcoupling to Navier-Stokes is achieved through the change in fluid geometry which is enforced by the conditions for the `MeshSolver`.

```

Name = FSI
Nonlinear Elasticity

```

```

FSI BC = on
Navier-Stokes
  NoSlip Wall BC = on
Mesh Update 1 = Equals Displacement 1
Mesh Update 2 = Equals Displacement 2

```

Now we are ready to choose the boundaries

Model

```

Set boundary properties
  Choose inlet side -> set boundary condition Inflow
  Choose outlet side -> set boundary condition Outflow
  Choose upper and lower sides (three pieces) -> set boundary condition Walls
  Choose obstacle base -> set boundary condition Base
  Choose interface between fluid and solid (two pieces) -> set boundary condition FS

```

For the execution ElmerSolver needs the mesh files and the command file. We have know basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

Sif

```

Generate
Edit -> look how your command file came out

```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case. It's a good idea to give the project an illuminating name. Avoid paths which includes empty spaces since they may cause problems later on.

File

```

Save Project
  Make New Folder -> fsi_obstacle
  OK

```

After we have successfully saved the files we may start the solver

Run

```

Start solver

```

A convergence view automatically pops up showing relative changes of each iteration. The simulation may take around 10 seconds depending on your platform.

The computed norms should be around 0.514 for the Navier-Stokes solver, 0.108 for the elasticity solver, and 0.0548 for the mesh update solver. These are reached after 18 iterations using the rather strict default settings.

If there is some discrepancy the setup of the system was probably different from the one in the tutorial. If the results are in agreement we are ready to look at the results.

## Results

To visualize the results open the postprocessor, in this case ElmerPost After the simulation has terminated we may open the postprocessor to view the results.

Run

```

Start postprocessor

```

A standard way of visualizing is to choose ColorMesh and there choose Surface or Both and the desired field variable, for example Velocity\_abs or Pressure. The mesh deformation is not active in all output formats. To activate the deformation in ElmerPost you may enter the following sequence of command to the command line at the bottom of ElmerPost window.

```
math n0=nodes
math nodes=n0+Displacement
```

The maximum speed in the system is around 2.328 and the maximum displacement 0.2636. Note that for the saved results the displacement and mesh update fields have been merged into one. In Figures 11.2, 11.3, and 11.4 the obtained velocity, pressure and displacement distributions are presented in the deformed mesh.

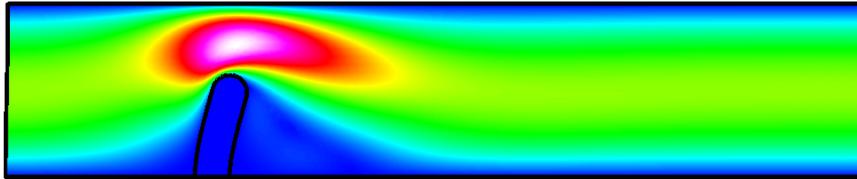


Figure 11.2: Velocity distribution of the obstacle in channel case.



Figure 11.3: Pressure distribution of the obstacle in channel case.

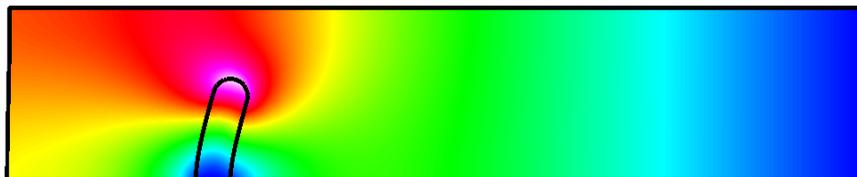


Figure 11.4: Displacement distribution of the obstacle in channel case.

## Tutorial 12

# Transient flow and heat equations – Rayleigh-Benard instability

**Directory:** RayleighBenardGUI

**Solvers:** HeatSolve, FlowSolve

**Tools:** ElmerGUI

**Dimensions:** 2D, Transient

### Case definition

This tutorial is about simulating the developing of the Rayleigh-Benard instability in a rectangular domain (Figure 12.1) of dimensions 0.01 m height and 0.06 m length. The simulation is performed with water and the material parameters of water required by the Elmer model are presented in Table 12.1. The temperature difference between the upper and lower boundary is set to 0.5 so that lower one has the temperature of 293.5 K and the upper one has the temperature of 293 K.

The density of water is inversely proportional to its temperature. Thus, heated water starts to flow upwards, and colder downwards due to gravity. In this case we assume that the Boussinesq approximation is valid for thermal incompressible fluid flow. In other words, the density of the term  $\rho \vec{f}$  in the incompressible Navier-Stokes equation can be redefined by the Boussinesq approximation

$$\rho = \rho_0(1 - \beta(T - T_0))$$

where  $\beta$  is the heat expansion coefficient and the subscript 0 refers to a reference state.

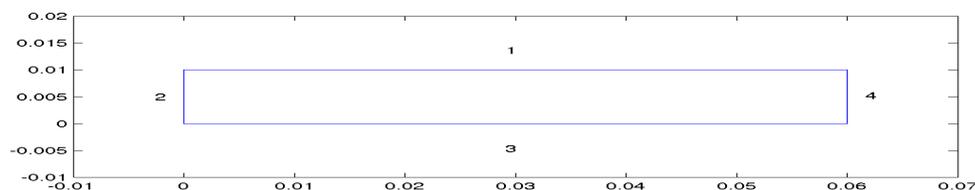


Figure 12.1: Domain.

Table 12.1: Material parameters for water

parameter	value
density	998.3 kg/m <sup>3</sup>
viscosity	1040e-6 Ns/m <sup>2</sup>
heat capacity	4183 J/(kg·K)
heat conductivity	0.58 W/(m·K)
heat expansion coefficient	2.07e-4 K <sup>-1</sup>
reference temperature	293 K

## Solution procedure

The mesh is given in ElmerGrid format in file `rectangle.grd`, load this file.

File

```
Open -> rectangle.grd
```

You should obtain your mesh and may check that it consists of 3036 bilinear elements.

There is a possibility to divide and unify edges to simplify the case definition in the future.

Choose (left wall + right wall (Ctrl down)) -> unify edge

After we have the mesh we start to go through the Model menu from the top to bottom. In the Setup we choose things related to the whole simulation such as file names, time stepping, constants etc. The simulation is carried out in 2-dimensional cartesian coordinates. 2nd order bdf time-stepping method is selected with 200 steps and with step size of two seconds.

Model

Setup

```
Simulation Type = Transient
Steady state max. iter = 20
Time Stepping Method = bdf
BDF Order = 2
Time Step Intervals = 200
Time Step Sizes = 2.0
Gravity = ...
```

In the equation section we choose the relevant equations and parameters related to their solution. In this case we'll have one set of equations (named "Natural Convection") which consists of the heat equation and of the Navier-Stokes equation.

When defining Equations and Materials it is possible to assign the to bodies immediately, or to use mouse selection to assign them later. In this case we have just one body and therefore its easier to assign the Equation and Material to it directly. It is important to select the convection to be computed since that couples the velocity field to the heat equation.

The system may include nonlinear iterations of each equation and steady state iterations to obtain convergence of the coupled system. It is often a good idea to keep the number of nonlinear iterations in a coupled case low. Here we select just one nonlinear iteration for both equations. For the linear system solvers we are happy to use the defaults. One may however, try out different preconditioners (ILU1,...) or direct Umfpack solver, for example.

Model

Equation

```
Name = Natural Convection
Apply to Bodies = 1
Heat Equation
```

```

Active = on
Convection = Computed
Edit Solver Setting
  Nonlinear System
    Max. iterations = 1
Navier-Stokes
  Active = on
  Edit Solver Setting
    Nonlinear System
      Max. iterations = 1
Add
OK

```

The Material section includes all the material parameters. They are divided to generic parameters which are direct properties of the material without making any assumptions on the physical model, such as the mass. Other properties assume a physical law, such as conductivities and viscosity.

Here we choose water at room temperature from the material library. You may click through the material parameters of the various solvers to ensure that the properties are indeed as they should be. Any constant set of units may be used in Elmer. The natural choice is of course to perform the computations in SI units.

Apart from the properties from the material database, we reference temperature for the Boussinesq approximation.

```

Model
  Material
    Material library
      Water (room temperature)
    General
      Reference Temperature = 293
    Apply to Bodies = 1
  Add
  OK

```

A Body Force represents the right-hand-side of a equation. It is generally not a required field for a body. In this case, however, we apply the buoyancy resulting from heat expansion as a body force to the Navier-Stokes equation.

```

Model
  Body Force
    Name = Buoyancy
    Apply to Bodies = 1
    Navier-Stokes
      Boussinesq = on
  Add
  OK

```

Initial conditions should be given to transient cases. In this case we choose a constant Temperature field and an small initial velocity that initializes the symmetry break.

```

Model
  Initial Condition
    Name = Initial Guess
    Heat Equation
      Temperature = 293
    Navier-Stokes
      Velocity 1 = 1.0e-9
      Velocity 2 = 0.0

```

Only one boundary condition may be applied to each boundary and therefore all the different physical BCs for a boundary should be grouped together. In this case the Temperature and Velocity. The side walls are assumed to be adiabatic.

Model

```
BoundaryCondition
  Name = Bottom
  Heat Equation
    Temperature = 293.5
  Navier-Stokes
    Velocity 1 = 0.0
    Velocity 2 = 0.0
  Add
  New

  Name = Top
  Heat Equation
    Temperature = 293
  Navier-Stokes
    Velocity 1 = 0.0
    Velocity 2 = 0.0
  Add
  New

  Name = Sides
  Navier-Stokes
    Velocity 1 = 0.0
    Velocity 2 = 0.0
  Add
```

The conditions may also be assigned to boundaries in the Boundary condition menu, or by clicking with the mouse. Here we use the latter approach as that spares us of the need to know the indexes of each boundary.

Model

```
Set boundary properties
  Choose Bottom -> set boundary condition Bottom
  Choose Top -> set boundary condition Top
  Choose Sides -> set boundary condition Sides
```

For the execution ElmerSolver needs the mesh files and the command file. We have now basically defined all the information for ElmerGUI to write the command file. After writing it we may also visually inspect the command file.

Sif

```
Generate
Edit -> look how your command file came out
```

Before we can execute the solver we should save the files in a directory. The project includes all the files needed to restart the case.

File

```
Save Project
```

After we have successfully saved the files we may start the solver

Run

```
Start solver
```

A convergence view automatically pops up showing relative changes of each iteration.

When there are some results to view we may start the postprocessor also

Run

Start postprocessor

## Results

Due to the number of the time-steps the simulation may take around ten minutes. You may inspect the results with ElmerPost as the time-steps are computed, or wait until all timesteps have been computed. When opening the result file using ElmerGUI ElmerPost only opens the first time-step. Therefore it is important to reopen the file and load the time-steps of interest. Pressing the button `All` selects all the calculated time steps. A video of the results can be viewed by selecting the option `Timestep Control` and pressing the button `Loop` under the `Edit` menu.

In Figures 12.2 and 12.3 the obtained temperature distribution and the velocity vectors are presented. The maximum velocity in the system should be about 0.516 mm/s.

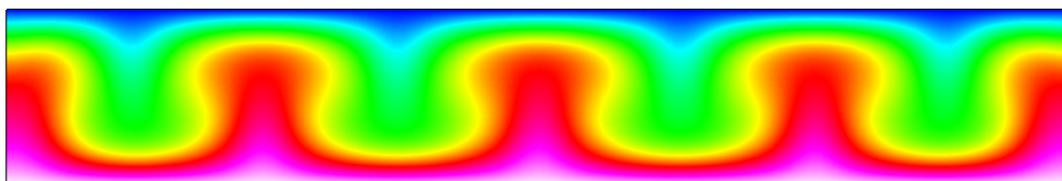


Figure 12.2: Temperature distribution at 260 s.

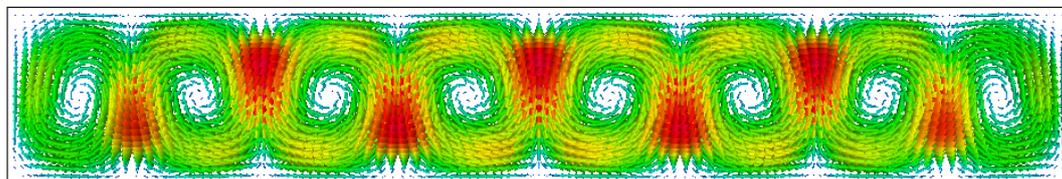


Figure 12.3: Velocity vectors at 260 s.

### Extra task: Sensitivity to temperature difference

If you have time you may try to solve the case with different parameters. Changing the temperature difference is one way of affecting the instability of the system. Decreasing the temperature differences the system eventually becomes steady state and the convection rolls vanish altogether. Increasing the temperature difference may increase the number of convection rolls and eventually the system becomes fully chaotic. Note that changing the temperature difference also affects to the time scale of the wake.